

University of California, Irvine

2025 Car Number(s)

2025 Vehicle: "Corsair"



School Name

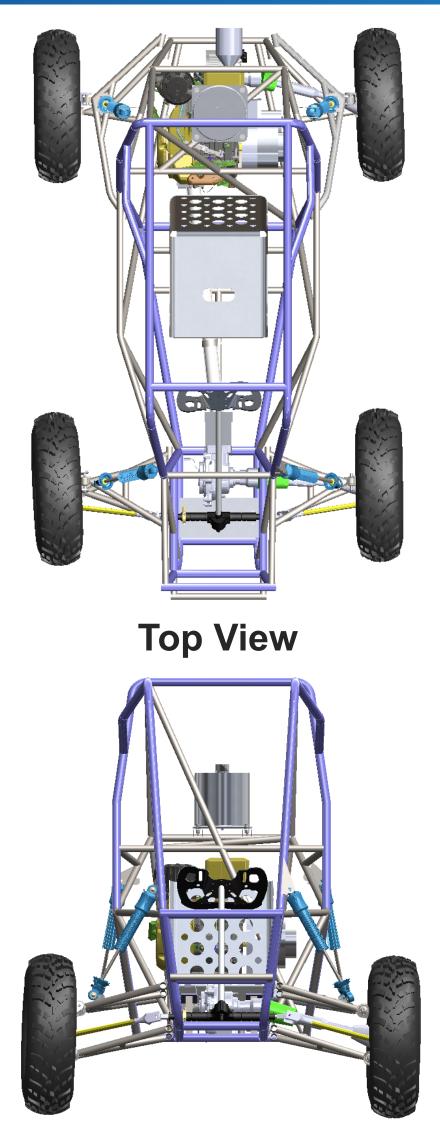






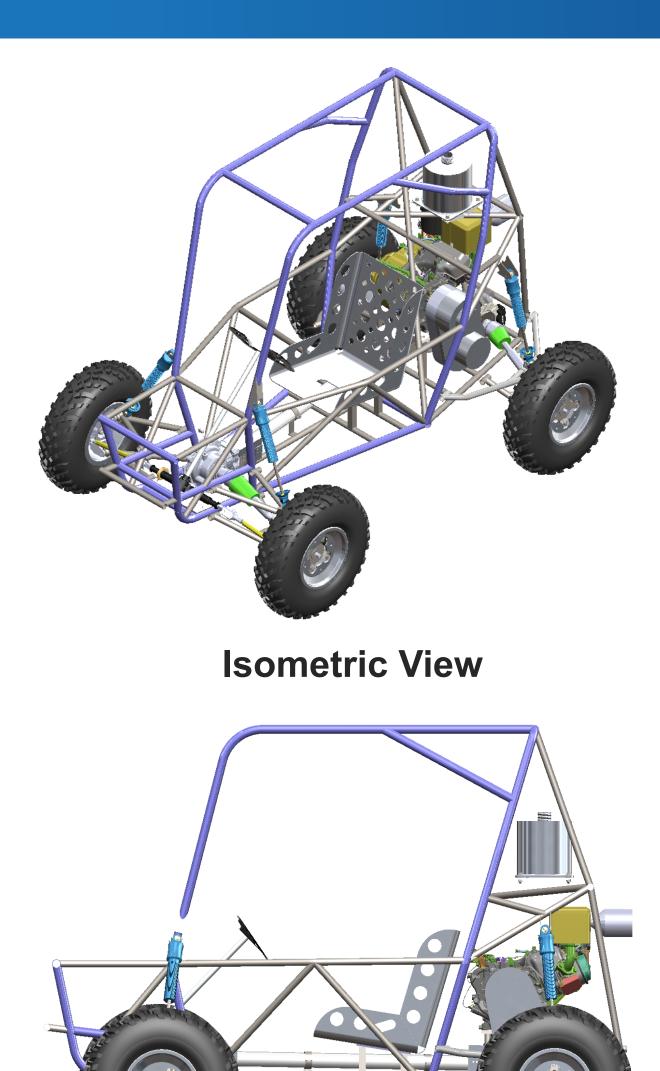


Corsair Master CAD



Front View





Side View







Team Goal

Competition History to Team Goals

Event Results	2023 California: (ABR23) "Rogue"	2024 California: (ABR24)	2025 Arizona: (ABR25)
		"Scoundrel"	"Corsair"
Business Presentation	39th	15th	Top 20
Cost Event	58th	39th	Тор 20
Design	41st	15th	Тор 20
Acceleration	31st	33rd	Тор 20
Hill Climb	48th	36th	Top 20
Maneuverability	DNF	17th	Тор 20
Suspension	42nd	30th	Тор 20
Endurance	46th	36th	Тор 20
Overall	56th	30th	Тор 20

Worsen Needs Work Improved



Goals For 2025 Competition		
Pass Tech Inspection	•	
Complete all events		
Score consistently across all events*		

Become a **competitive top 20 team***

Steps To Success

- Maximize scores on dynamic events
 - Overall system weight reduction
 - Improve key component durability and subsystem reliability
 - Refined vehicle with subsystem packaging
- Maximize scores on static events

amic Events	Points
eleration	70
Climb or Traction	70
d Maneuverability	70
pension or Rock Crawl	70
urance	400
al	680

tic Events	Points
sign Evaluation	150
st Evaluation	100
siness Presentation	70
al	320

Fig. 1 Competition Score Breakdown



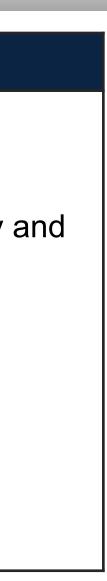
Fig 2. 2023 Team at Washougal, OR



Fig 3. 2024 Team at Gorman, CA















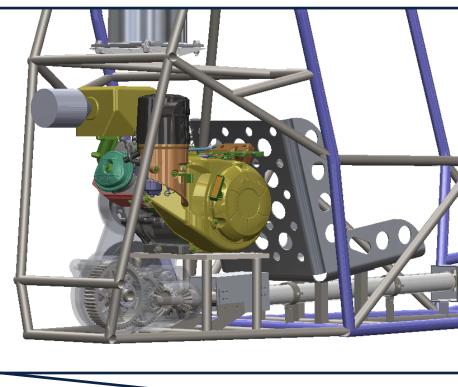
System Design

Subsystem Specification and Integration

 Table 1: System Direction Design

Sub-Team	Major Subsystem Changes		
Chassis and Body	 Optimize chassis size using more accurate human models 		
Powertrain (Transmission)	 Custom Transfer case for rear power delivery CVT Tuning 		
Powertrain (Driveline)	 Custom driveshaft for weight reduction 		
Suspension and Steering	 Introduce front rake to absorb front impacts 		
Brakes and Human Interface	 Introduce rear inboard brakes to lower sprung weight Lower seat height for CoG 		
Overall System ABR24 Weight 700 lbs w/o driver ABR25 Weight Goal: 500 lbs w/o driver ~ 30% Weight Reduction			

Fig. 1 Driveline/Transmission Integration



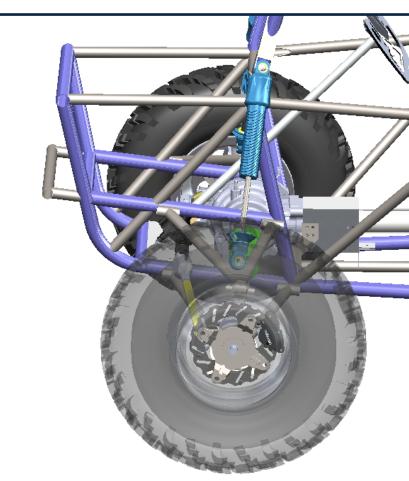


Fig. 2 Chassis/Suspension Integration



Fig. 3 Transmission/Brakes/Driveline Integration

> Fig. 4 Human Interface/Chassis/Driveline Integration









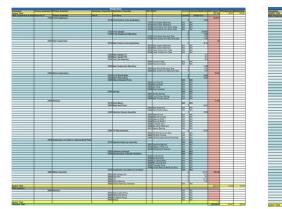


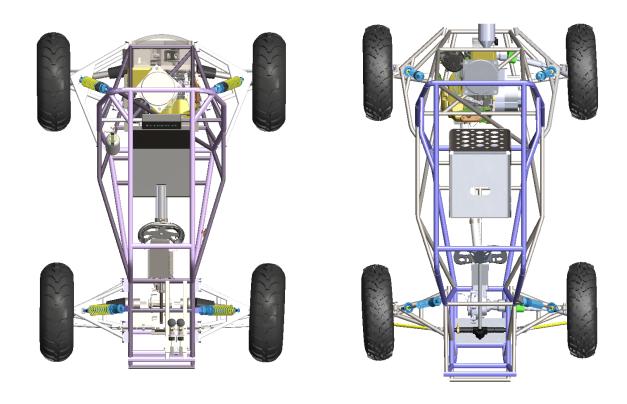


System Weight Study

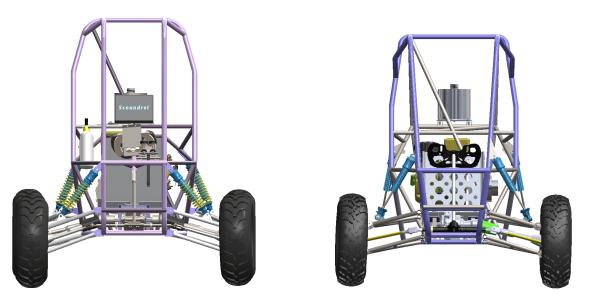
Lightest 4WD Baja Car Yet

Table 1: System Weight Results					
Sub-Team	ABR24 Weight w/o driver (lbs)	ABR25 Weight w/o driver (lbs)	ABR25 Weight Reduction %		
Brakes / HI	65.6	40.8	37.8%		
Chassis/Body	108.6	97.3	10.4%		
Powertrain	306.9	148.6 (Trans.) 100.3 (Drive.)	18.8%		
Suspension and Steering	229.5	166.	27.6%		
Total	710.5	558.1	21.4%		





Top View: ABR24 & ABR25 (TW 59" -> 55")

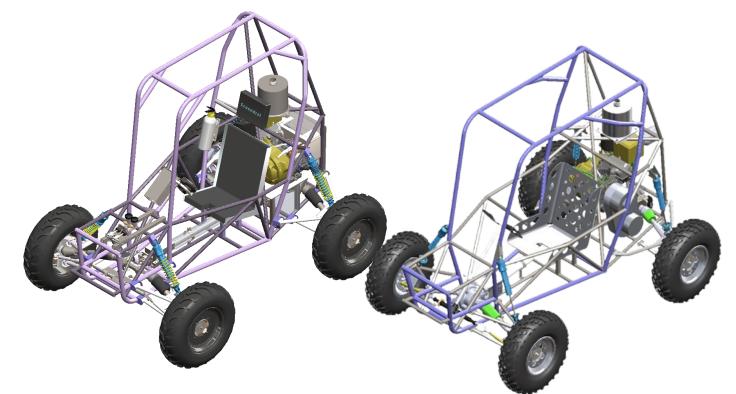


Front View: ABR24 & ABR25 (Height 67" -> 62")



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Fig 1: Organized Excel Spreadsheet tracking all subsystem weights



Iso View: ABR24 & ABR25



Side View: ABR24 & ABR25 (WB 56" -> 56.5")





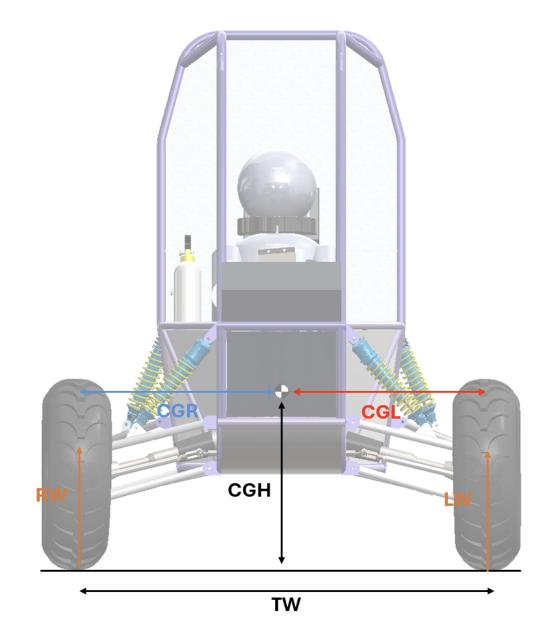




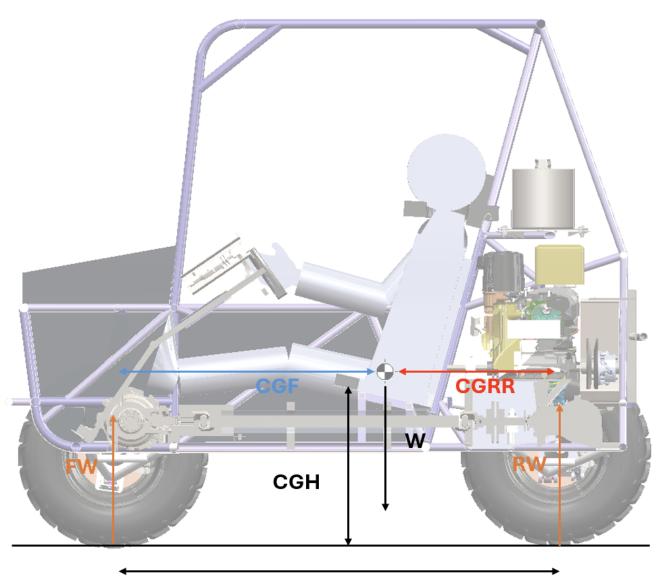




Weight and Balance Sheet









Side CoG View



How this applies: Roll moment



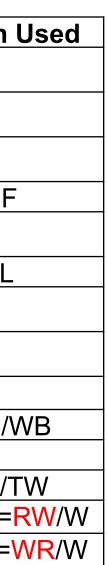
Weight Sheet and Corsair Targets

Parameter	Value	Unit	Equation
Weight (W)	850	lbf	
CG Height (CGH)	21.7	in	
CG from Front Axle (CGF)	34.3	in	
CG from Rear Axle (CGR)	21.6	in	=WB-CGF
CG from Left (CGL)	26	in	
CG from Right (CGR2)	26	in	=TW-CGL
Wheelbase (WB)	56	in	
Track Width (TW)	52	in	
Front Weight (FW)	329.4	lbf	=W-RW
Rear Weight (RW)	520.6	lbf	=W*CGF/V
Left Weight (WL)	425	lbf	=W-WR
Right Weight (WR)	425		=W*CGL/T
Weight Split Front%-Rear% (WSF-WSR)	38.75%	61.25%	= FW /W, = F
Weight Split Left%-Right% (WSL-WSR2)	50.00%	50.00%	= <mark>\/</mark> \/\/W, =\

Parameter	Scoundrel	Corsair
Front Roll Center	7.8 in	6.3 in
Rear Roll Center	7.5 in	6.8 in
CoG Height	21.7 in	Undefined
Ride Height	12 in	11 in



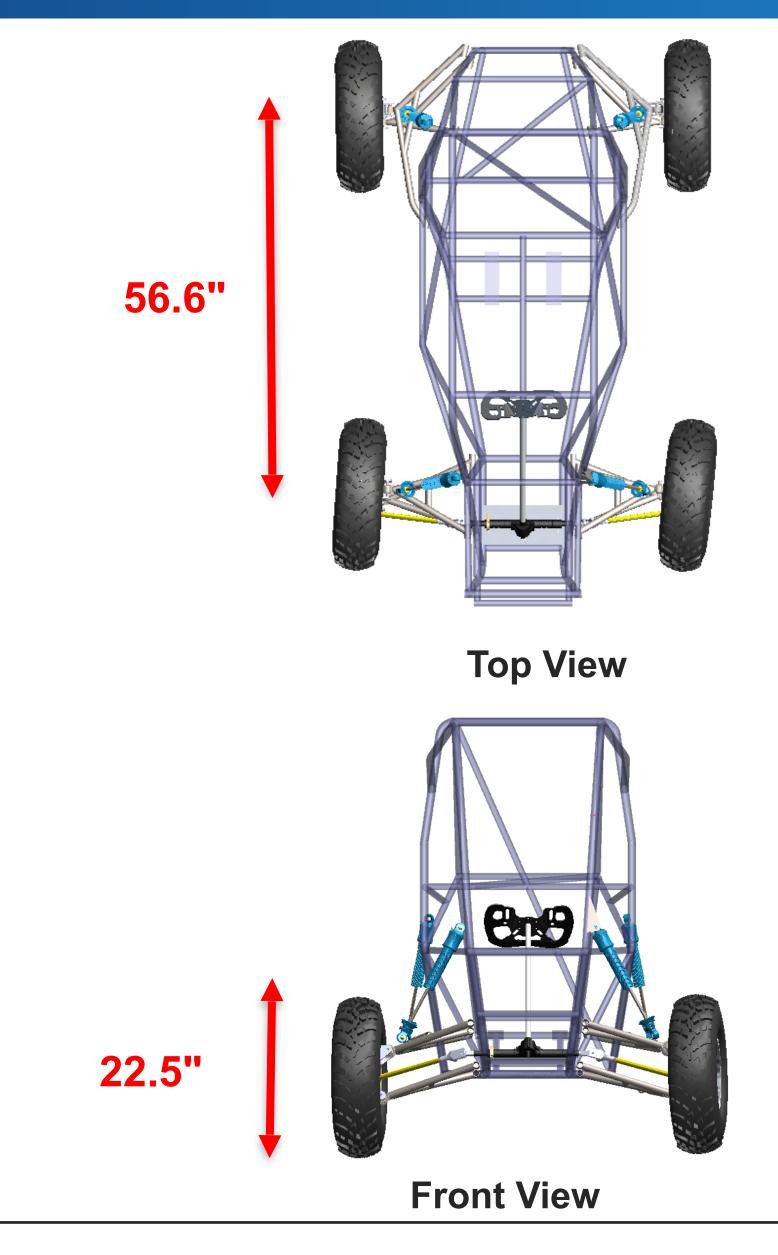




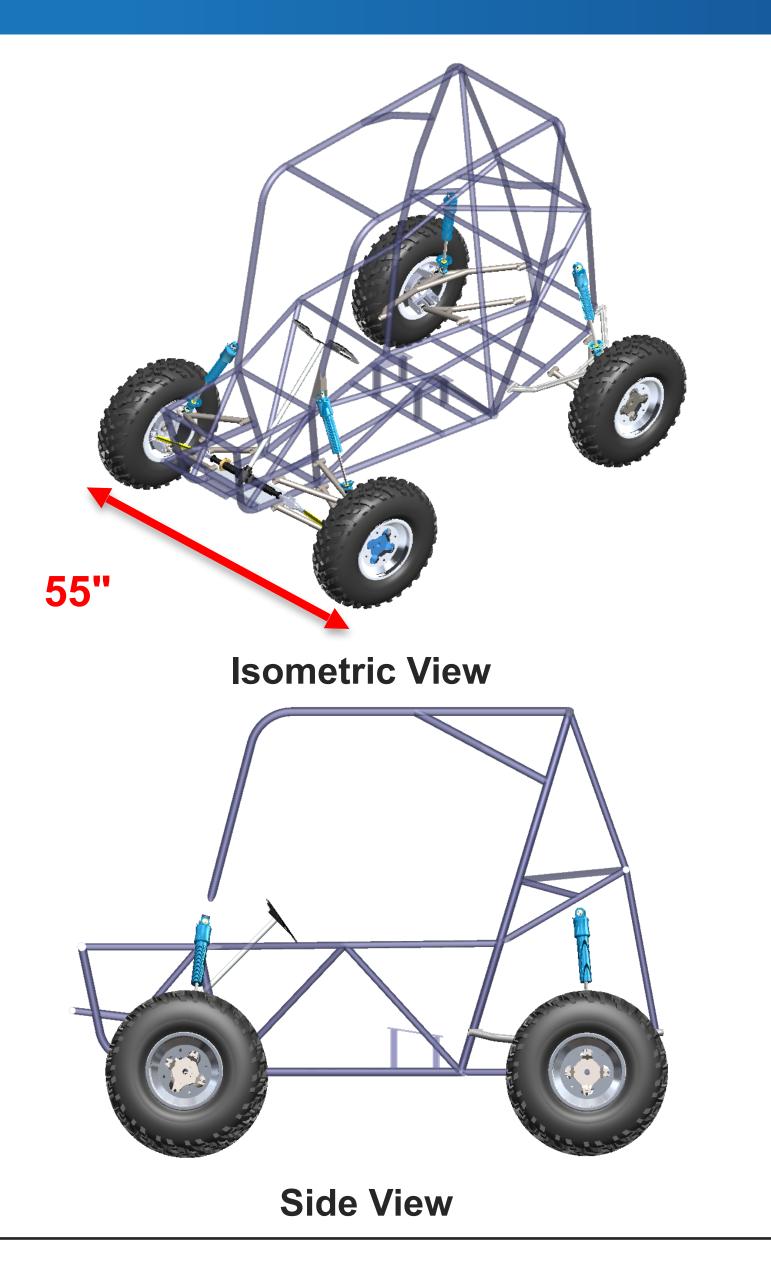
















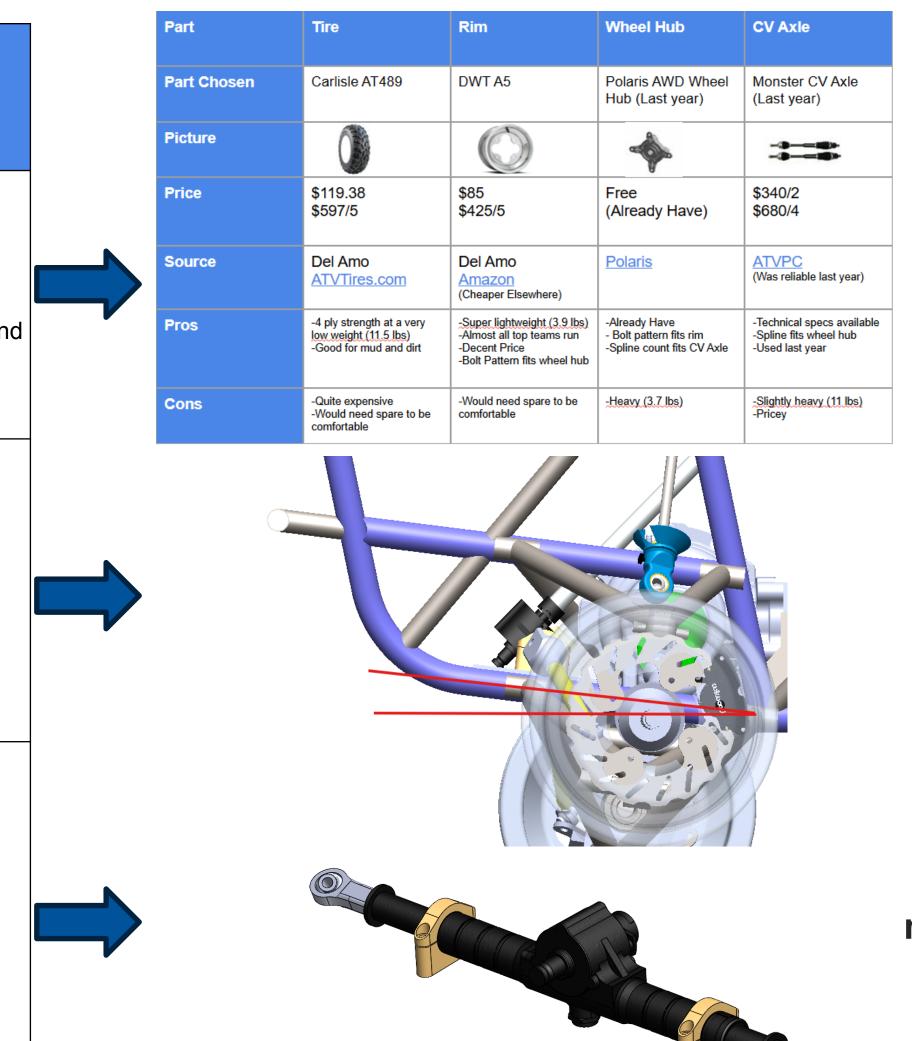




Overall 2025 System Goals	Why	How
Reduce Weight	 Overall goal for this years car 	 Choosing a lighter wheel/cv axle assembly Switch to aluminum front uprights Reducing control arm wall thickness and OD
Introduce Front Control Arm Rake/ Wheel Recessional Travel	 Allows us to get over obstacles with less initial speed (logs, rocks) Most of our recoveries from endurance were because of this, and that's what got us DQ'ed. Increased driver comfort All the top teams do this 	 Include inclination in our kinematic suspension analysis Collaborate with chassis to introduce an inclination in the toe box.
Stronger Steering System	 Rack extension failure on Scoundrel Steering arm failure on Scoundrel Rack mount had lots of flex Steering wheel popped out during endurance 	 Source a rack and pinion that fits our needs better. Better rack and pinion mounting, mounting includes braces for less bending Stronger steering arm Add shaft collars to steering column components to hold in place.



Meeting System Goals



Weight Savings: 53 lbs rotating unsprung mass **30% weight reduction**

7 degrees of Front **Suspension Rake**

Rack and Pinion mounts further apart to reduce bending moment arm













Suspension, Steering, and Shocks

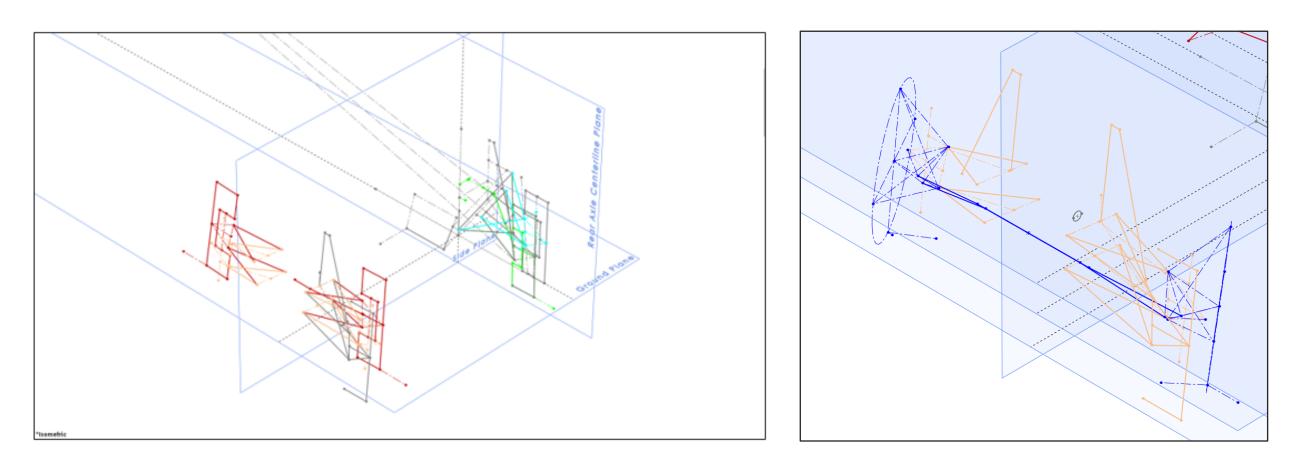


Fig 1: Suspension and Steering Kinematics & Shock Mounting determined using Solidworks

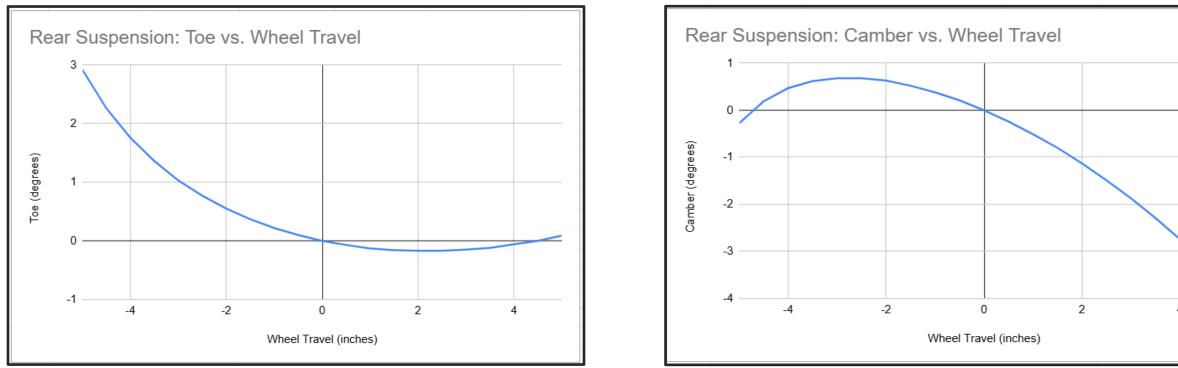


Fig 2: Camber and Toe Gain Graphs generated with Solidworks motion analysis to verify requirements are met





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Fig 3: AFCO 63 Series 7" Stroke Increased Motion Ratio vs Scoundrel

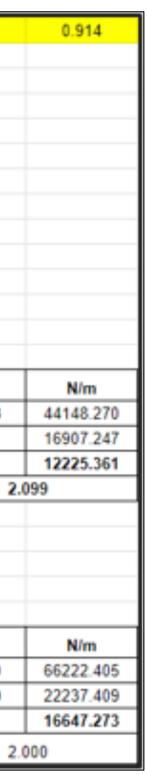
Rear Springs	LbF/in	Length (in)
K1	255	9
К2	180	5
Front Springs	LbF/in	Length (in)
K1	170	9
К2	100	5

Jump Height	3.000
Suspension Frequency Equation	
f =sqrt(K_total/M_corner)/2*pi	
- adult_totanin_contents2 pr	
Dual Active Springs Setting	
1/K_T = 1/K1 + 1/K2	
Frequency	2.000
Front Spring Constants	Lbf/in
K1 (Main Spring)	252.093
K2	96.543
K_total	69.809
Calculated Frequency	
Rear Spring Constants	Lbf/in
K1 (Main Spring)	378.140
K1 (Main Spring) K2	126.979
KT	95.058
Calculated Frequency	
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Fig 4: Spring Rate Calculator used to determine spring rates



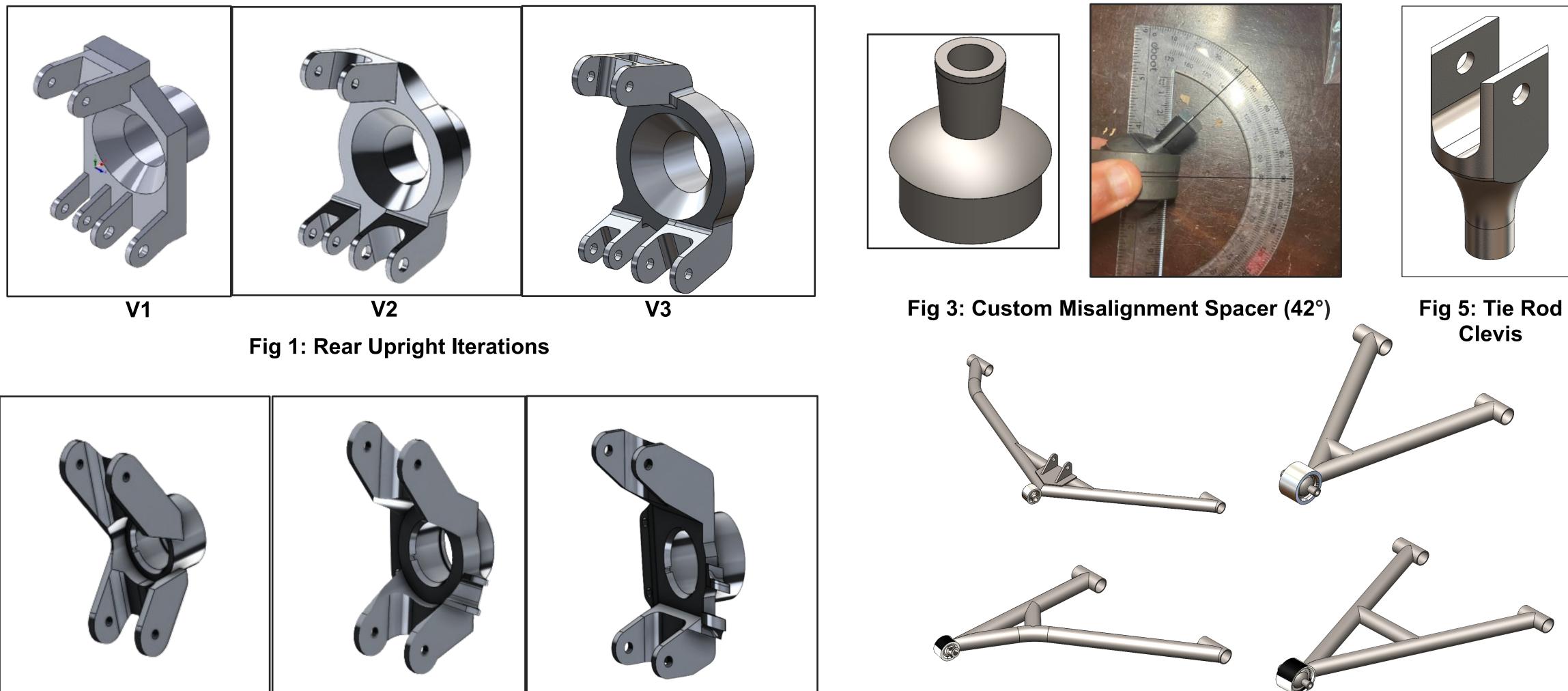


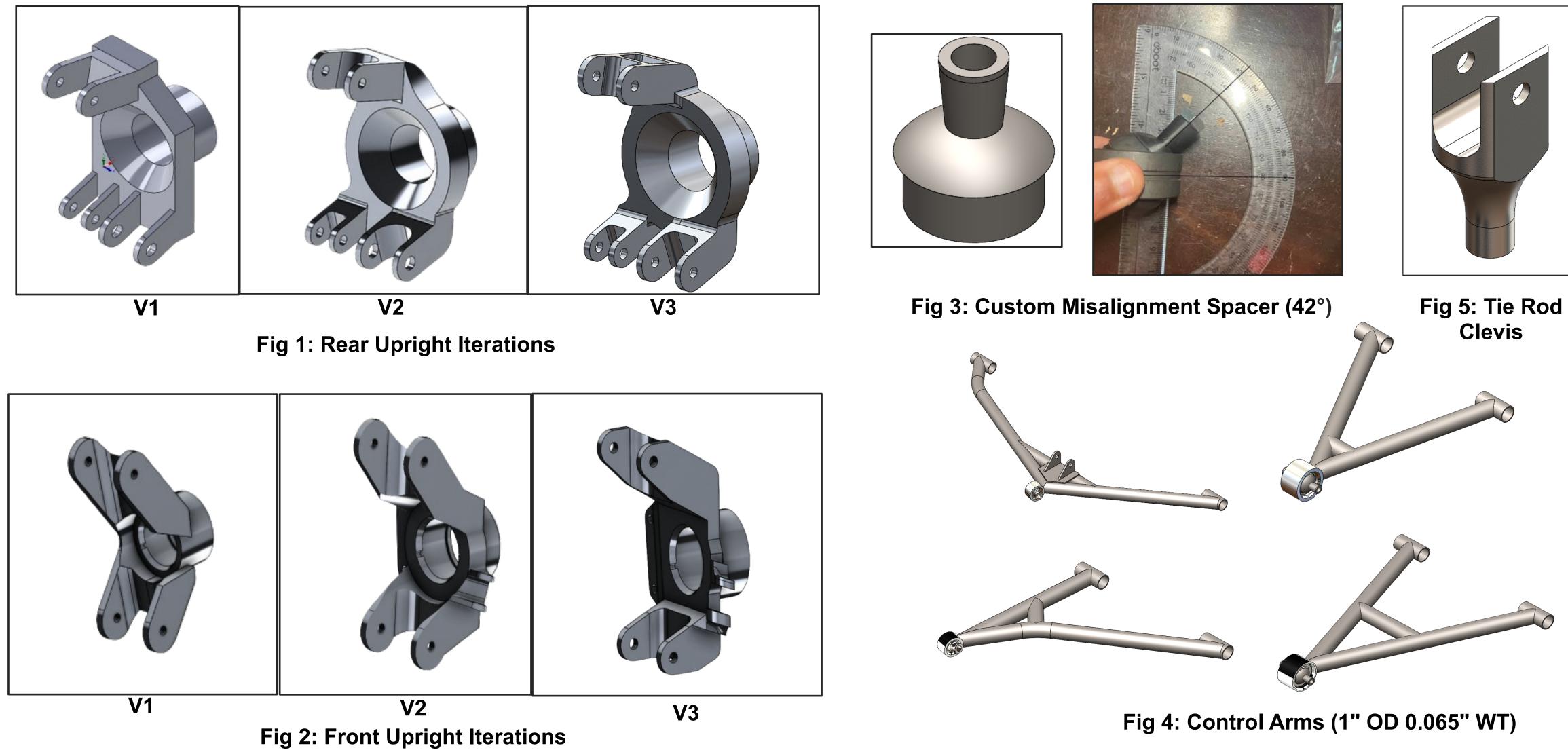






Design of Custom Components















Dynamic Calculations

Minium Braking Distance (x)

Dynamic Mass Transfer (DNT Vertical Load from Unsprung (VLU)

Force on Caliper Mounting (FC)

NEED TO SOLVE SYSTEM OF EQUATION

Upper Mounting Reaction Force (F1)

Lower Mounting Reaction Force (F2)

Vertical Load on Each Wheel (VLEW) Vertical Force from Centrifugal (VLC)

Vertical Force from Gyroscopic (ELG)

Upper Mounting Reaction Force (F3)

ower Mounting Reaction Force (F4)

Maximum Deceleration (a)

Total Vertical Load (TVL)

Frictional Force (FF)

Braking Torque (BT)

Lateral Forces

Lateral Force

Velocity at Turns

Net Vertical Force (NVF)

Braking Torque

Top Speed (V)

Dynamic Condition

SUSPENSION AND STEERING

FEA of Custom Components

	Inputs	Value	Unit	Formula
Load	Shear Force (V)	2000	lbf	
	Tensile Force (F)	200	lbf	
Fastener	Yield Stress (Y)	85000	psi	
	Minor Diameter (MD)	0.2458	in	
	Torque Spec (T)	20	ft*lb	
	Double Shear?	~		
Calculations	Effective Shear (EV)	1000	lbf	
	Bolt Minor Area (A)	0.04745	in^2	PI/4 * MD^2
	Preload (P)	2016.706	lbf	0.5*Y*A
	Tensile Total Force (FT)	2216.706	lbf	P+F
NASA Fastener Criterion	Von Mises Shear Yield (SY)	49045	psi	0.577 * Y
	Rs	0.429686		(EV/A)/SY
	Rt	0.549586		(FT/A)/Y
	Passes Criterion?	TRUE		Rt^2+Rs^3<=1
MAE 150 Von Mises Criterion	Shear Stress (SS)	21073.97	psi	EV/A

Unit Equation

4.89 ft/s^2 a = V/(-2x)

77.79 lbf =TUM/4

211.20 lbf =nu*TVL 202.40 lbf*ft =FF*TR

971.53 lbf =BT/CMR

507.38 lbf =FF-F2

29.33 ft/s 20 mph 155.00 lbf =TSM/2+TUM/4

455.55 lbf =nu*NVF

981.60 lbf =LF+F3

Unit

281.60 lbf =DNT+TVL

203.81 lbf =((C*ROGF+M*a*COG)/WB)/

-296.18 lbf =(-FC*TOSA+FF*CTLA)/(CTLA-

261.25 lbf =(M*V^2*COG)/(2*TGR*TW)

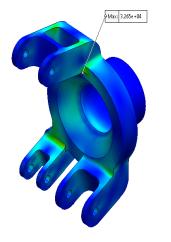
607.40 lbf =sum(VLEW:VLC)

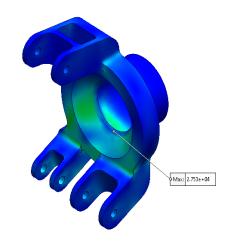
191.15 lbf =(4*MEW*TR^2/2)*((V^2/(TR*TGR))

-526.05 lbf =LF*(TR-CTUA)/(CTUA+CTLA)

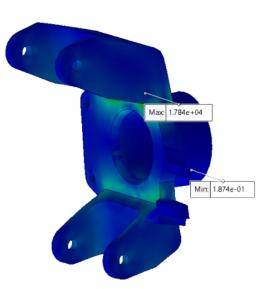
29.33 ft/s

3.00 ft





Bump Force 81% Yield Stress



Bump Force 11% Viold Stross

Lateral Force 64% Yield Stress

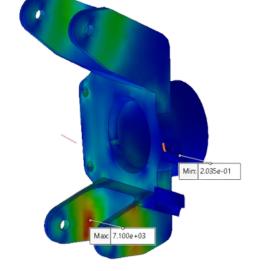
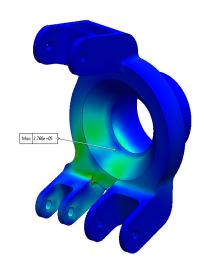


Fig 2: Upright FEA, 6061 T6 Aluminum

						41% field Stress
teering Calculations						
puts			Calculations			
escription	Value	Unit	Steering Effort			
leight of Vehicle (W)	600	lbf	Description	Value	Unit	Equation
Front Weight Distribution (%FW)	40	%	Front Corner Weight (FCW)	120.0	b lbf	(W/%FW)/2
ront Suspension Rake (FSR)	7	deg	Mechanical Trail (MT)	0.1	3 ft	WD/2 * sin(CA)
crub Radius (SR)	1.8	inches	Lateral Force (LF)	0.0	b lbf	(W"V*2)/R
teering Arm Longitudinal Length (SAL)	2.32	inches	Lateral Torque (LT)	0.0) lb*ft	LF*MT
aster Angle (CA)	8	deg	Shock Vertical Force (SF)	122.2	5 lbf	(MSS*MSSL + SSS*SSSL)* sin(SMA) * cos(FSR)
/heel Diameter (WD)	23	inches	Friction Force (FF)	193.8	lbf	µ*(FCW+SF)
ie Rod Length (TRL)	13.73	inches	Friction Torque (FT)	29.0	7 Ibf"ft	FF*SR
ie Rod Lateral Distance(TRLaD)	13.59	inches	Combined Torque @ KP (CT)	29.0	7 Ibf"ft	FT+LT
ie Rod Vertical Distance (TRVD)	1.65	inches	Force on TerRod Force To Rack (FTR)	150.3	5 lbf	CT/SAL
ie Rod Longitudinal Distance (TRLoD)	1.07	inches	F5 Steering Column Torque (SCT)	6.6	1 Ibf"ft	FTR*(PGD/2)
ornering Speed (V) (Set to 0 for static steering)	0	mph	Steering Effort	14.4	9 Ibf	SCT/SWD
ornering Radius (R)	10	ft	Impact Scenario			
riction Coefficient (µ)	0.80	unitiess	Constant Deceleration (CD)	88.0	2 ft/s^2	S/D
inion Gear Diameter (PGD)	1.06	inches	Force on Tire (FoT)	1627.9	lbf	(W/g)*CD*cos(FSR)
teering Wheel Diameter (SWD)	11	inches	Torque to Kingpin (TK)	447.6	7 lbf*ft	FoT*(SR+x in)
			Resultant Force (RF)	2315.5	5 Ibf	TK/SAL
npact Scenario			Tie Rod Unit Vector (TRUV)			
ehicle Speed (S) (or speed difference Vi-Vf)	15	mph	Tie Rod Lateral Vector (TRLV)	0.9) unitiess	TRLaD/TRL
luration of Impact (D)	0.25	sec	Tie Rod Vertical Vector (TRVV)	0.1	2 unitiess	TRVD/TRL
			Tie Rod Longitudinal Vector (TRLV)	0.0	3 unitless	TRLoD/TRL
			Tie Rod Axial Force	2291.9	4 164	RF * TRLV

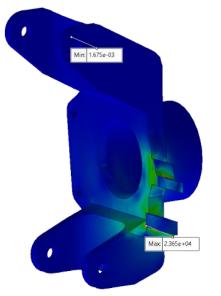
Fig 1: Calculators used to determine loadings





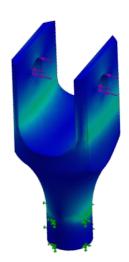
Toe Link Force 41% Yield Stress

Rock Impact Scenario 94% Yield Stress



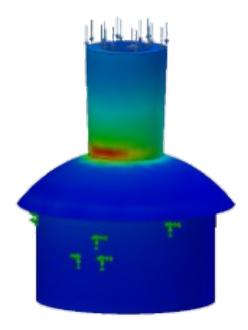
Lateral Force 74% Yield Stress

Steering Arm Force 60% Yield Stress



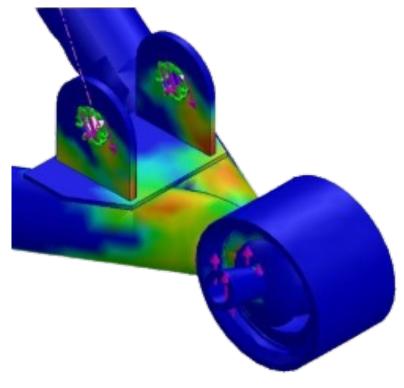
Tie Rod Force 48% Yield Stress

Fig 3: Tie Rod Clevis FEA **1020 Steel**



Bump Force 72% Yield Stress

Fig 4: Misalignment Spacer FEA, 630 Stainless



Bump Force 80% Yield Stress

Fig 5: Control Arm FEA, 4130 **Chromoly Steel**



















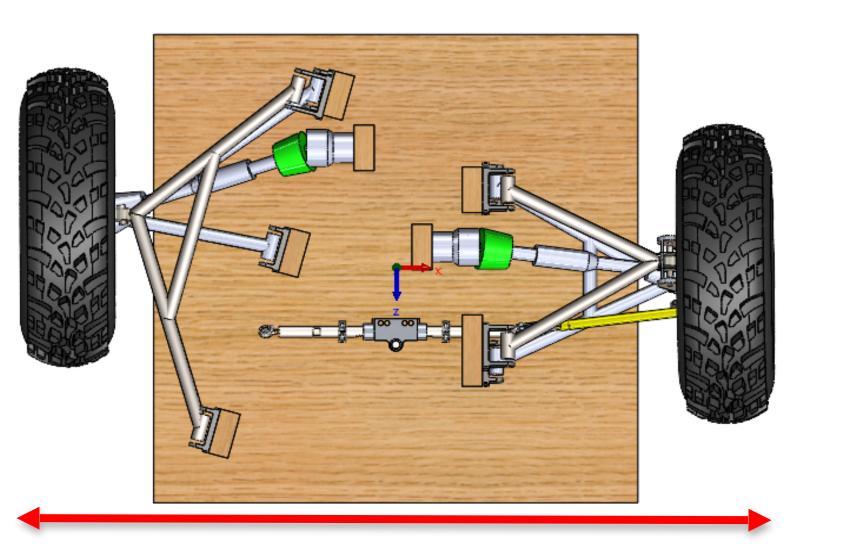




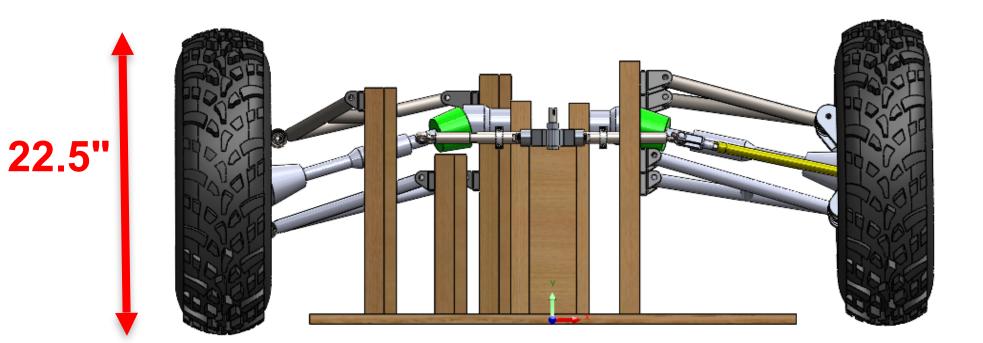




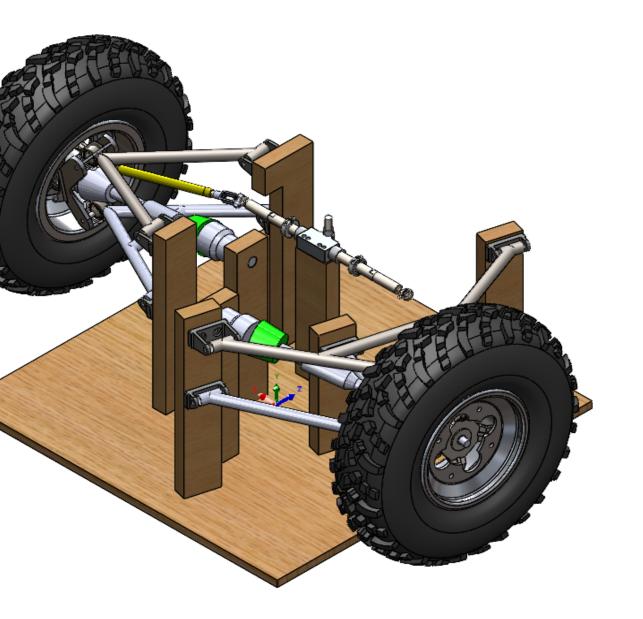
Suspension Prototype











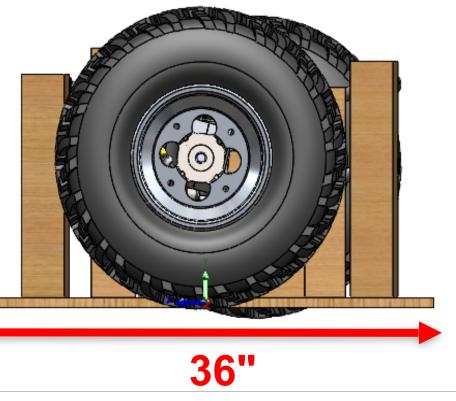
Suspension Prototype Goals

<u>Verify:</u> Toe Gain Camber Gain Wheel Vertical Travel Wheel Recessional Travel

Steering Geometry

- Wheel turning angles 0
- Ackermann % Ο

CV Axle articulation Misalignment Spacers Max Angle Manufacturing Tolerances









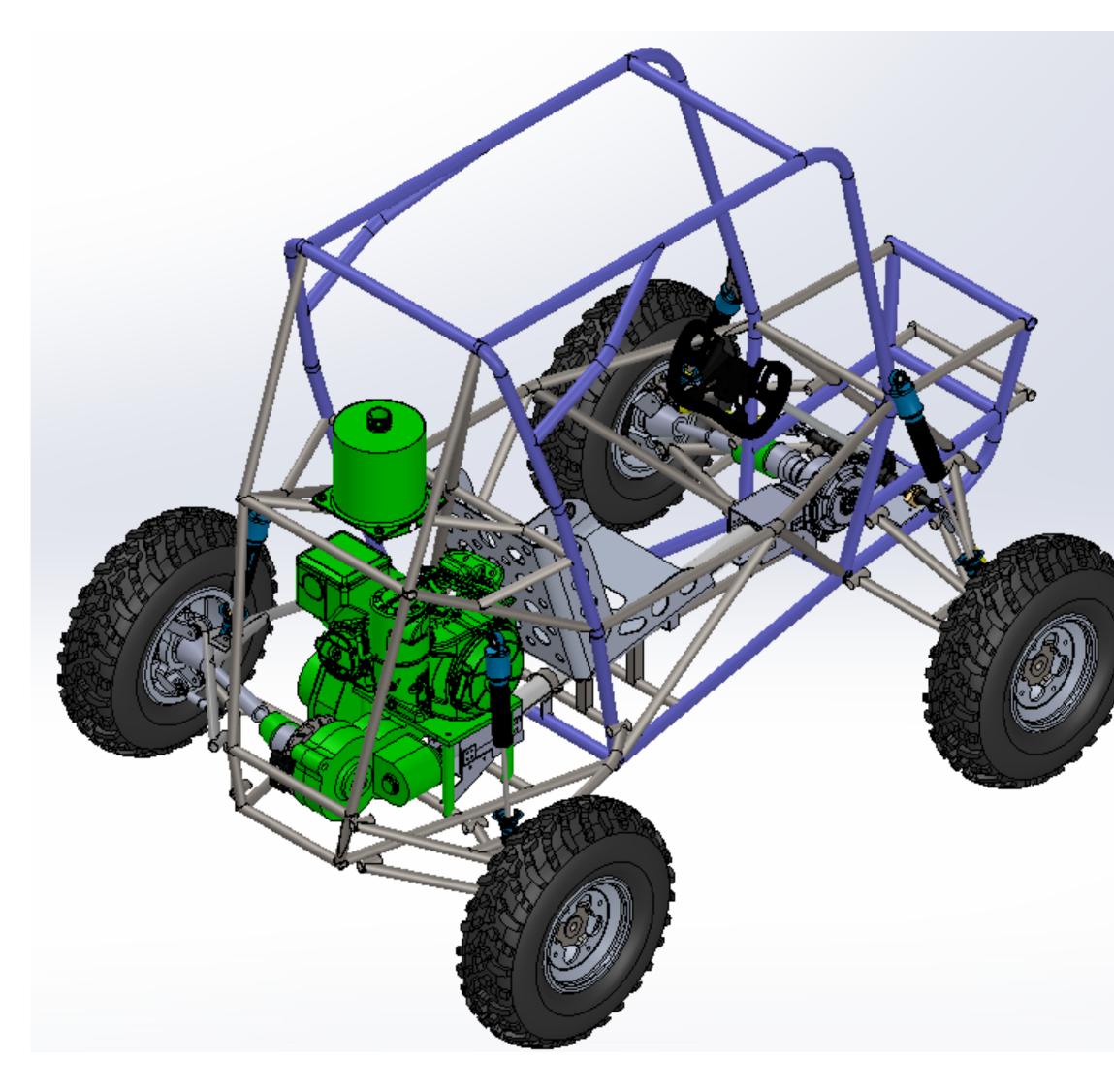






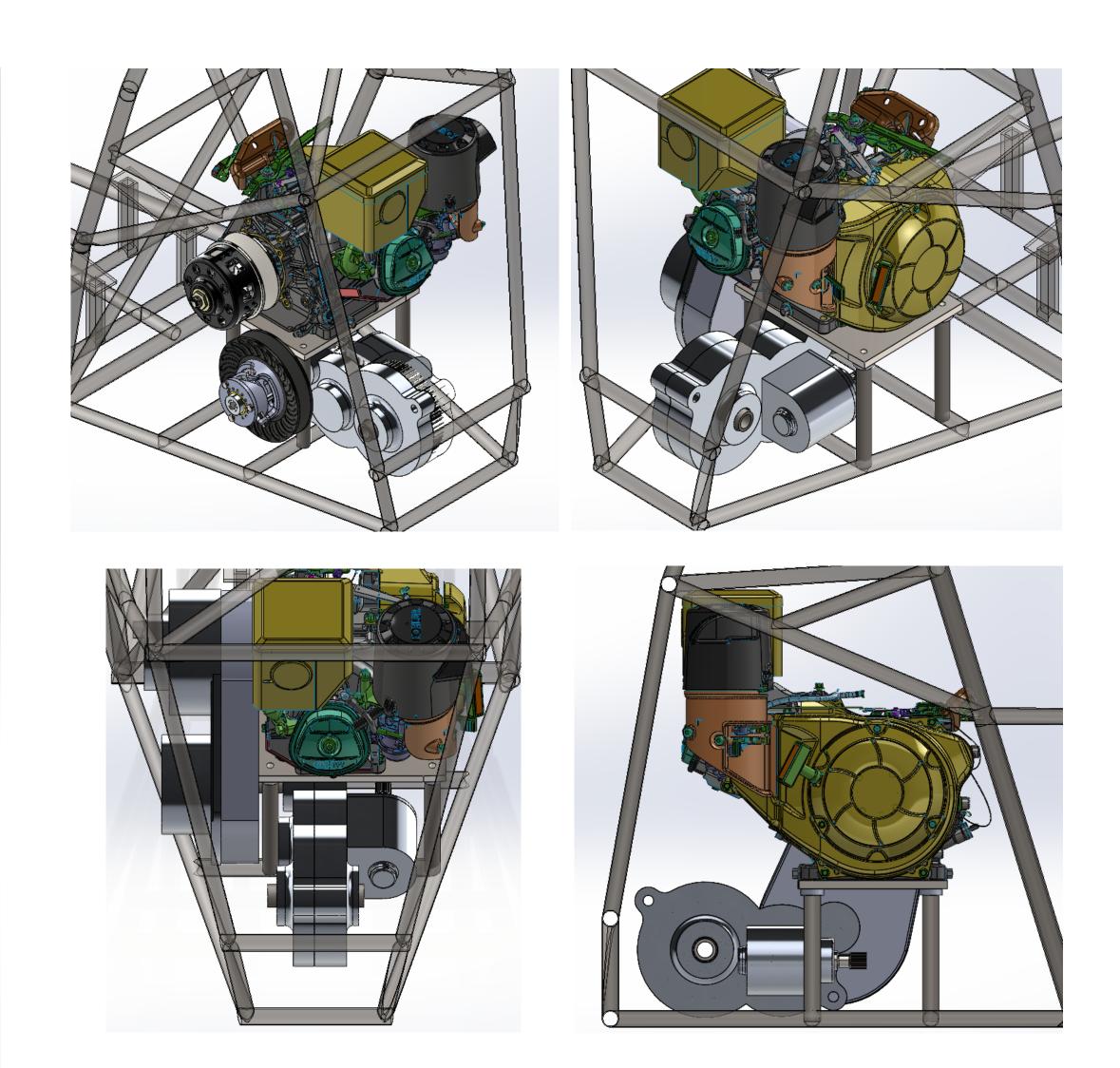


POWERTRAIN (TRANSMISSION)



Corsair Powertrain Transmission Subassembly





Transmission Packaging in Chassis







POWERTRAIN (TRANSMISSION)

Requirements

Description	Requirement	Reason
Vehicle Acceleration to complete 100 ft	< 4.5 s	Time to Place within top 20-25 teams
Top Speed	> 28 mph	Ensure sufficient torque and speed
Torque at Rear Wheels	> 597.2 ft-lb	Calculated to complete traction event
Overall Ratio (Rear)	32.28	Calculated to complete traction event
Transfer Case Ratio	8.28	Calculated to complete traction event
Transfer Case Weight	45.8 lbs	30% Reduction (From old transfer case + Differential)



Design Changes

	Scoundrel 2024	Corsair 2025
Transmission Weight	220.3 lbs	148.6 lbs (32.5% Reductio
Peak Torque at Rear Wheels (2WD)	543.5 ft-lbs	604.58 ft-lbs (11.2% Increas
Total Reduction (From CVT to Wheels)	7.5	8.3
Overall Ratio (Rear)	29.38	32.28
Hill Climb Angle	45°	76°

Main System Requirements:

- 1. Ensure all components can withstand aggressive and unpredictable off-road racing conditions
- 2. Increase torque delivery to wheels to complete all dynamic Baja SAE events
- 3. Decrease powertrain weight by 30% from previous years' vehicle, for a new total vehicle weight of ~650 lbs















POWERTRAIN (TRANSMISSION)

ANSI/AGMA 2001—D04 Gear Design

Transfer Case Gear Specifications					
	Teeth	Diametral Pitch (teeth/in)	Face Width (in)		
Gear 1	19	10	0.875		
Gear 2	55	10	0.875		
Gear 3	19	8	1.4375		
Gear 4	55	8	1.4375		
Bevel 1	19	6	0.6875		
Bevel 2	15	6	0.6875		

Gear	Factor of Safety for Wear "Sh"	Factor of Safety for Bending "Sf"		Factor of Safety for Wear "Sh"	Factor of Safety for Bending "Sf"
Gear 1	1.15	1.02	Gear 1	1.15	1.02
Gear 2	1.23	1.54	Gear 2	1.23	1.53
Gear 3	1.64	2.06	Gear 3	1.16	1.03
Gear 4	1.76	3.10	Gear 4	1.24	1.55
Bevel 1	1.57	1.02	Bevel 1		
Bevel 2	1.38	1.14	Bevel 2		

AWD Factors of Safety

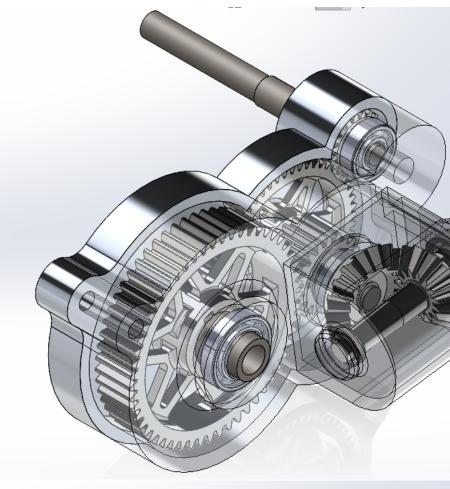
RWD Factors of Safety

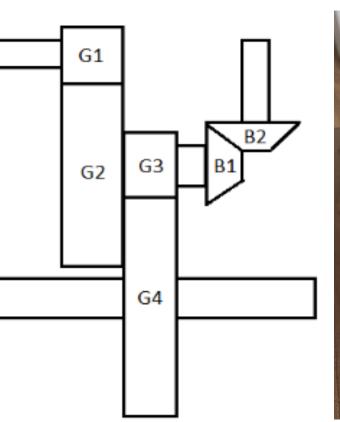
*AGMA FOS are calculated in addition to a 1.75 shock load factor



Transfer Case Design

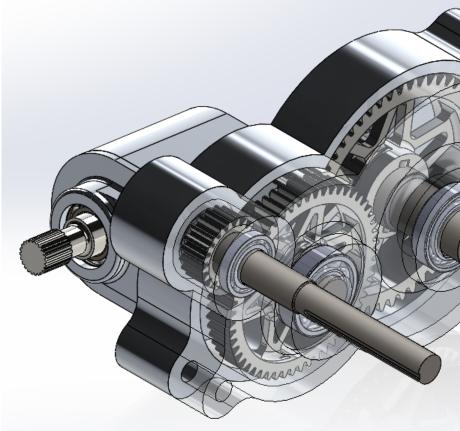
	Material
Gears	Grade 2 Carburized and Hardened 8620 Steel
Shafts	4340 Steel
Housing	6061 Aluminum







Gear Layout and 3D Printed Proof of Concept



Transfer Case Design





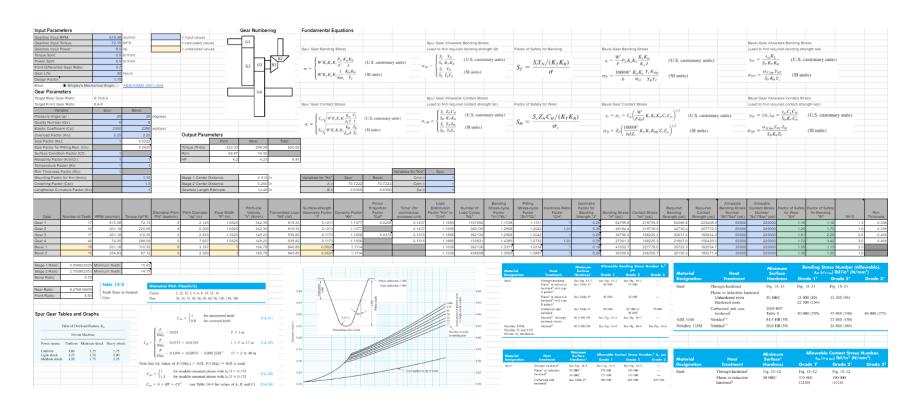




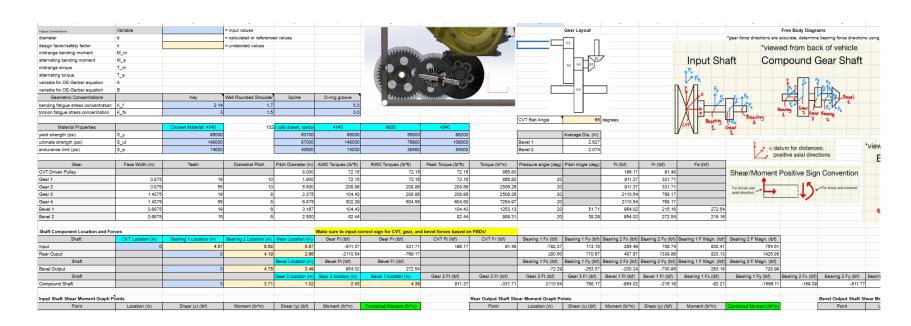




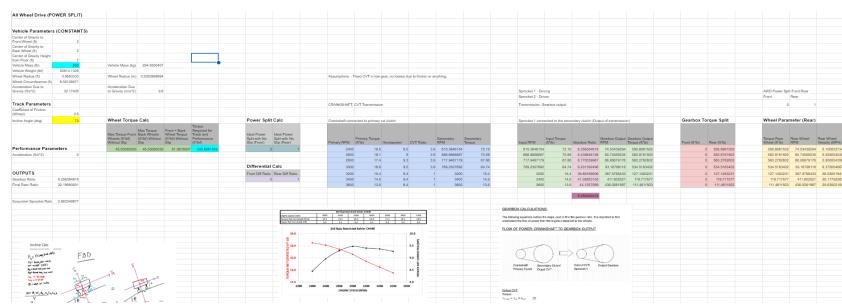
Transfer Case Calculations and FEA



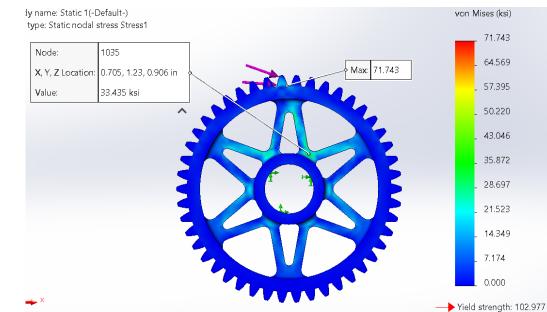
AGMA 2001—D04 Calculations

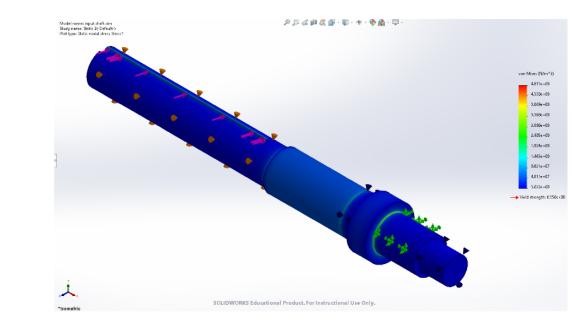


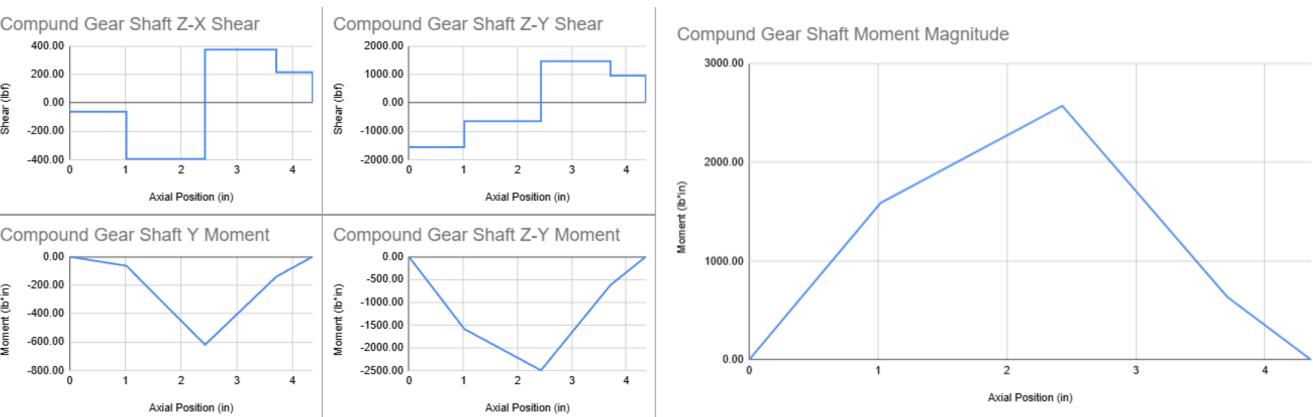
Shaft Calculations

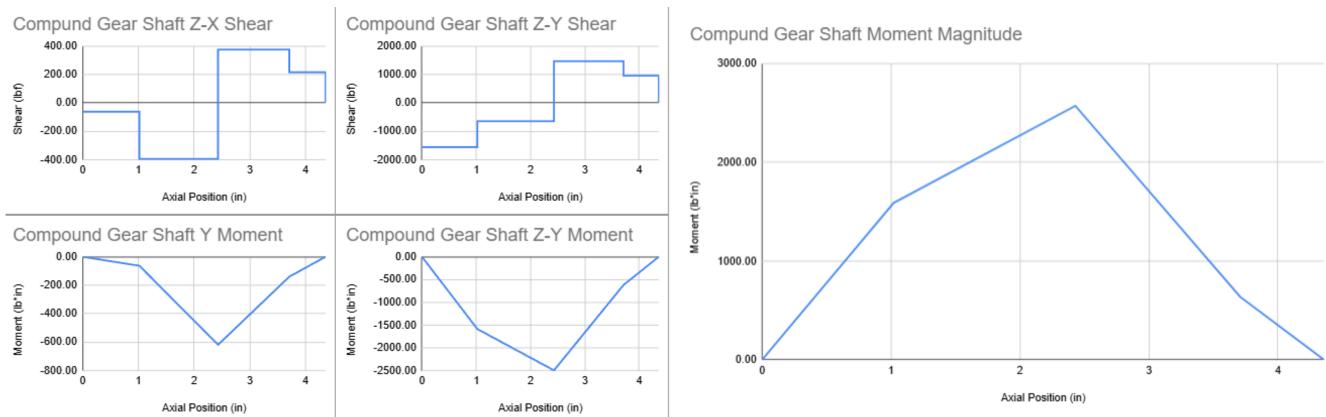


Performance/Ratio Calculations







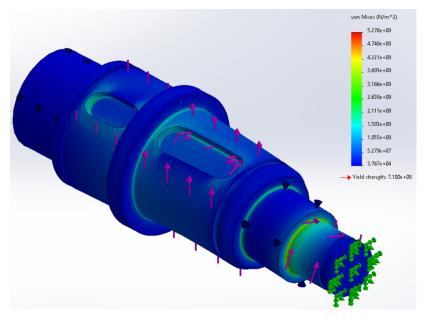




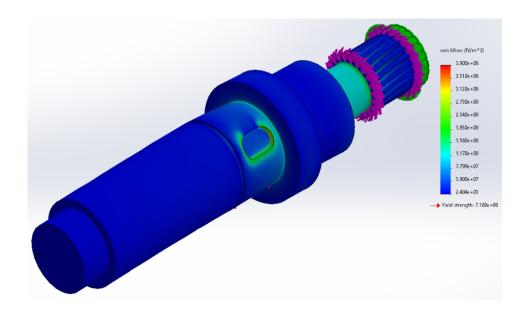


Gear Webbing Analysis

Input Shaft FEA



Compound Shaft FEA



Driveshaft Output FEA







16



Component	Scoundrel	Corsair
Guarding	Carbon Steel Hard to disassemble	6061 Aluminum Designed for manufacturing
Driveshaft	2" OD Unknown thickness	1.25" OD 0.083" wall thickness
Differentials	Reliable front differential Rear differential lost traction	Front Differential: Polaris Sportsman - On Demand 4WD

















Chromoly Steel (4130) 1.25" Diameter, 0.083" Wall Thickness Shaft

	Transmission Output Value	Driveshaft Maximum Value
Torque (lbf*ft)	82.4	505.7
Critical Speed (RPM)	269.3	6395.2

16% of torque capacity 4% of RPM capacity



Driveshaft Calculations

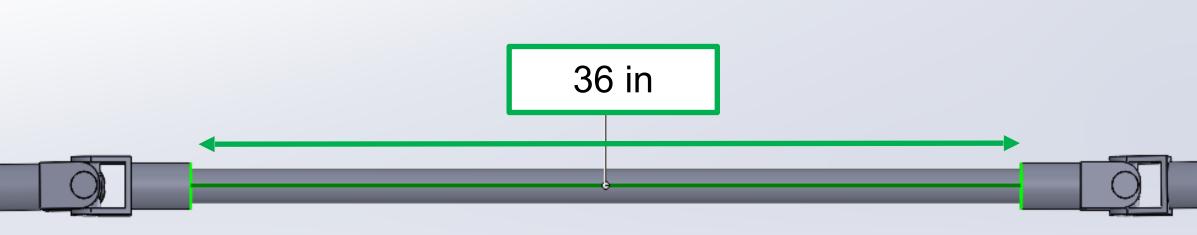


Fig 1: Driveshaft Extension Length

Material of choice						
Chromoly Steel (4130)						
Variables	Inputs		Properties of Interest	Values		
Shaft Outer Radius (m):	0.015875	(0.625 in)	Axial Stiffness (N/m):	180539920.6		
Wall Thickness (m):	0.002108	(0.083 in)	Torsional Stiffness (Nm/rad):	8747089.176		
Shaft Length (m):	0.899		Static Deflection:	0.000028943		
Shaft Mass (kg):	1.3855		Shear Stress (MPa):	40.93828702		
Engine Torque (Nm):	111.77		Maximum Torque (Nm):	685.6843132	SF:	6.13
Yield Stress of Shaft Material (MPa):	251.15		Bending Stress (Pa):	1960258.968		
Young's Modulus of Shaft Material (GPa):	205		Critical Speed (RPM):	5559.436967		
Poisson's Ratio:	0.29		Duty Cycle (Time):			
Shaft Density (kg/m^3):	7850					
Torsional Strength (Pa):			Max Allowable Shear Stress	72.45601541		

Fig 2: Driveshaft Calculator used to determine diameter and wall thickness













U-Joint Phasing

Side View Working Angle: 0.7°

Top View Working Angle: 5.75°

Estimated Driveshaft RPM: 270

DRIVESHAFT RPM	MAXIMUM OPERATING ANGLE
5000	3.2 [°]
4500	3.7°
4000	4.2 °
3500	5.0°
3000	5.8°
2500	7.0°
2000	8.7°
1500	11.5°

Fig 1: Operating Angle Verification, table taken from Autodata Training

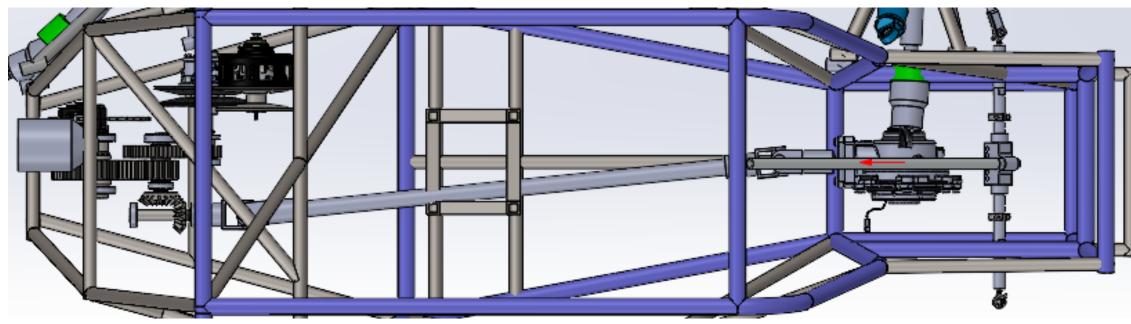


Fig 2: Corsair Top View



Driveline Clearance

Scoundrel: 6.4" from bottom member

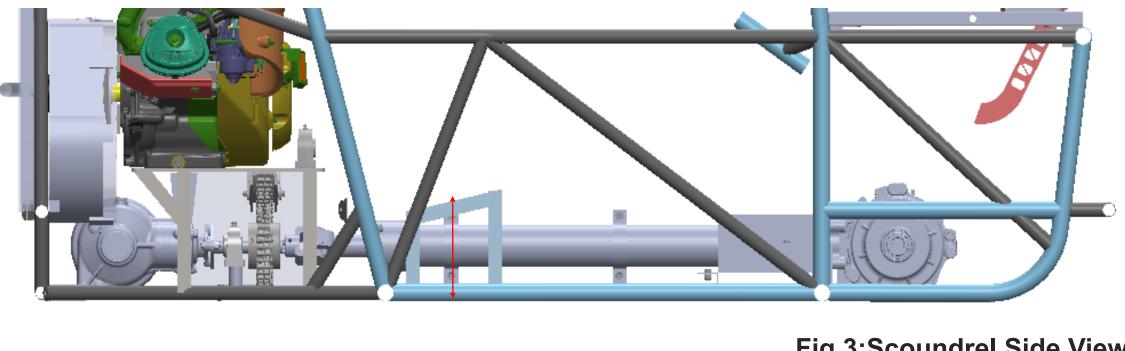
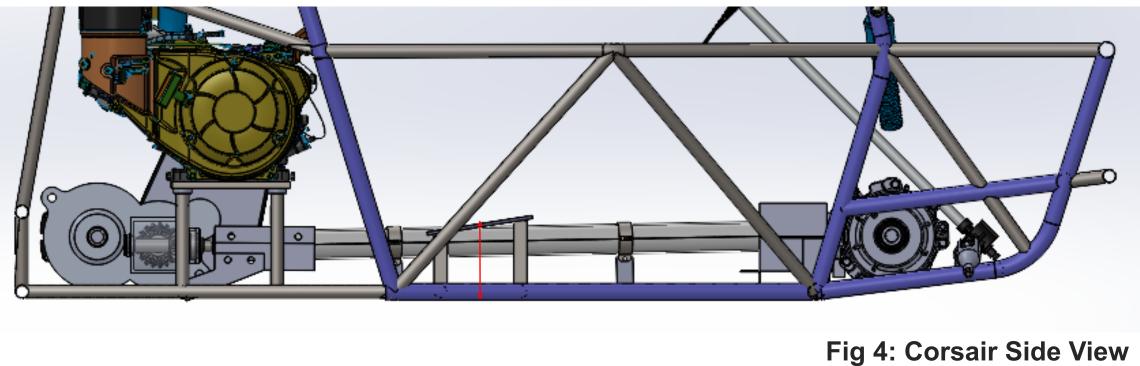


Fig 3:Scoundrel Side View

Corsair: 5.4" from bottom member







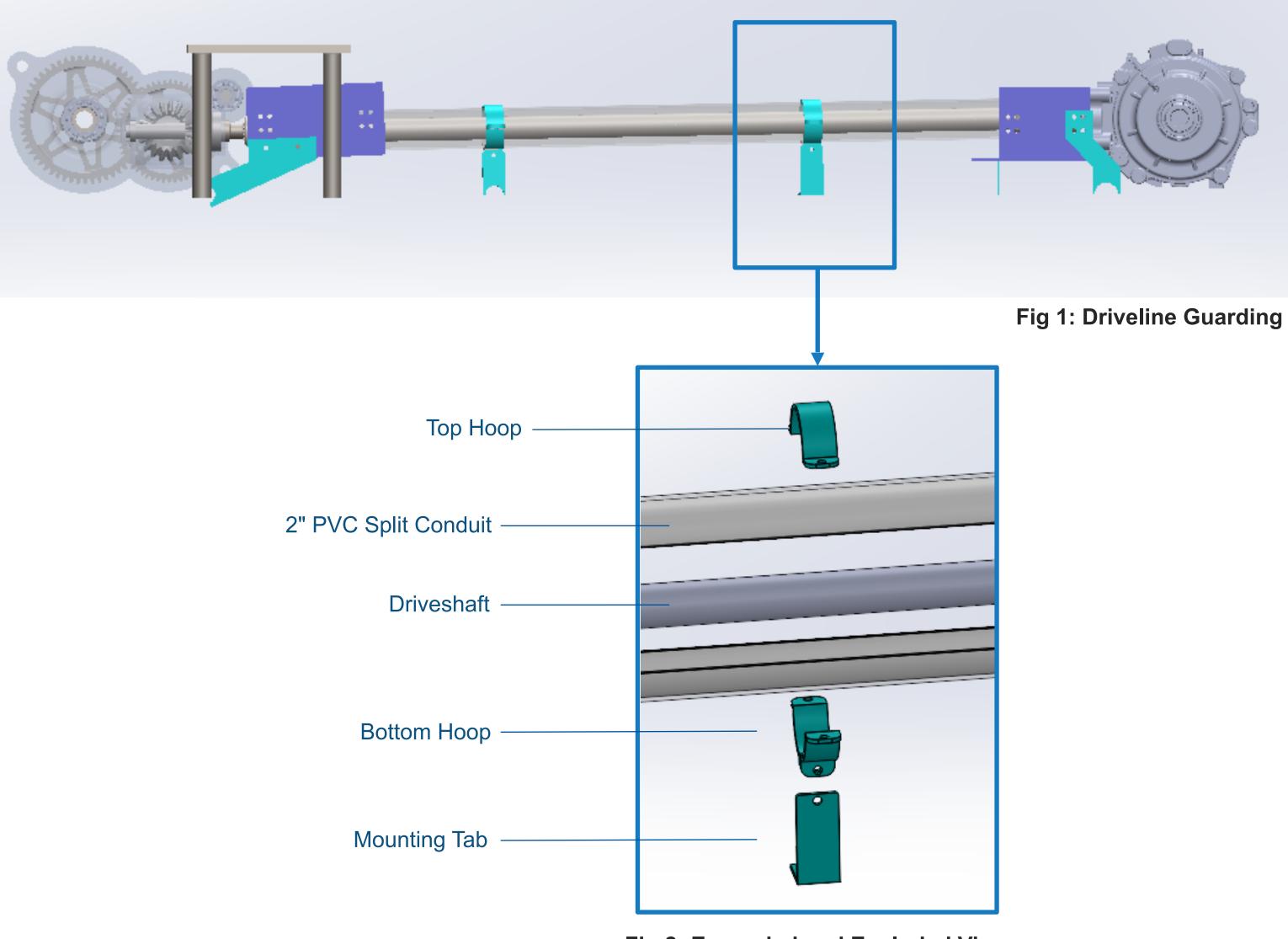




POWERTRAIN (DRIVELINE)

Yoke Guards

~60% weight reduction •



Driveshaft Guarding

1" diameter reduction ullet











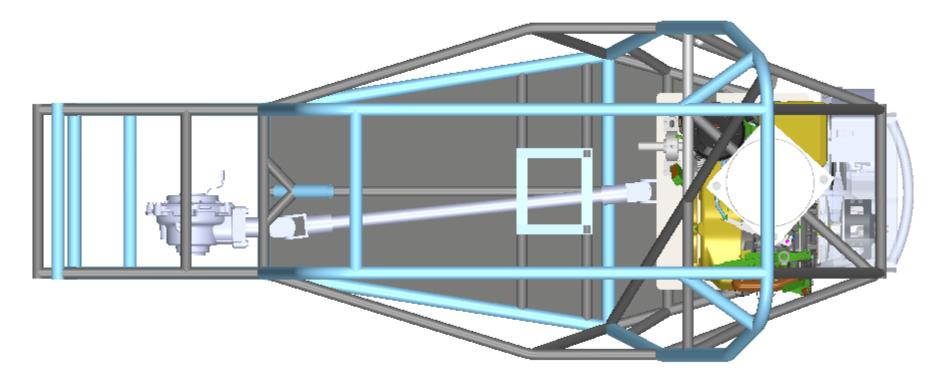




Driveline Subsystem Prototype

Testing Goals:

- Vibration testing
- Constant velocity verification
- Test at low (idle simulation), medium (typical driving speeds), high (peak operational range) speeds





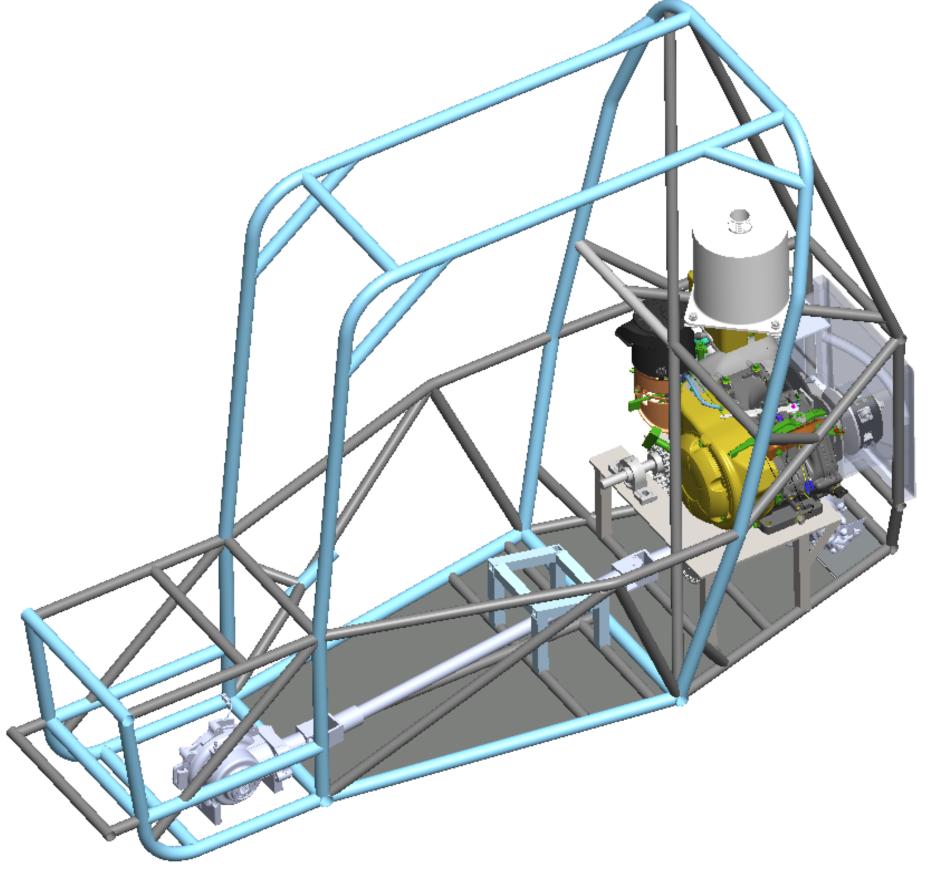


Fig 1: Scoundrel with New Driveline Geometry, Isometric View









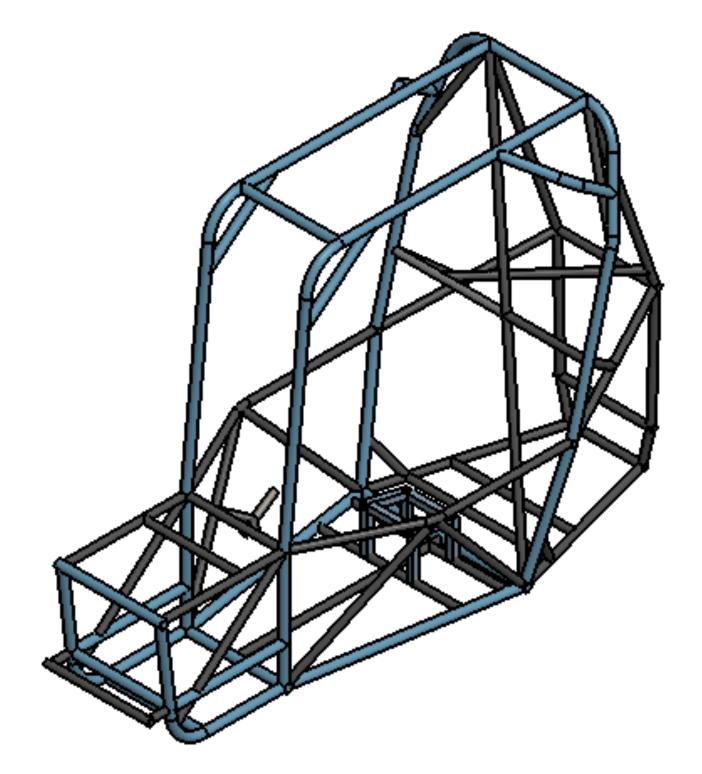




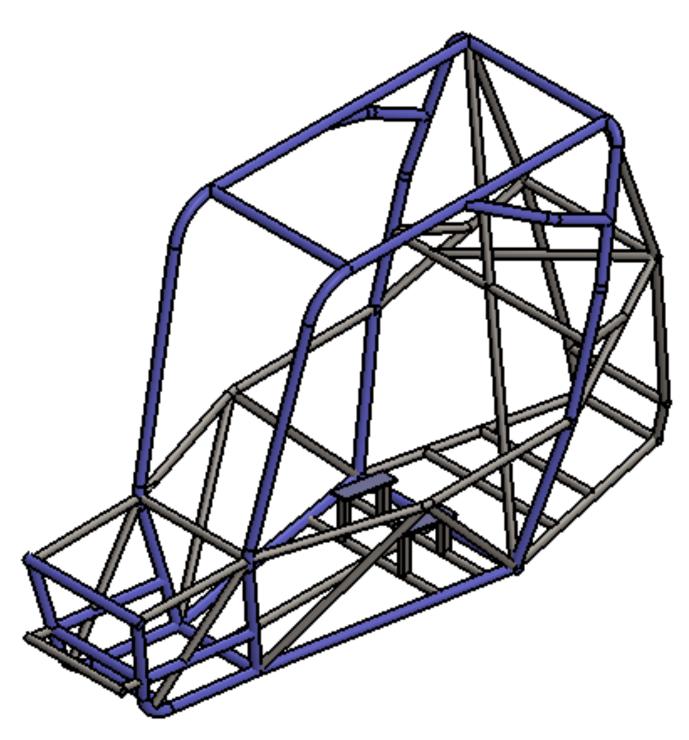
CHASSIS - Frame

Subsystem Goals

Subsystem Goal	Reason	Approach
Weight Reduction	Overall system goal	Reduce unnecessary members; simplify seat mount
Optimized Driver Accommodation	Prevent excess overhead clearance	Reduce chassis profile by designing around designated drivers
Maintain Ease of Manufacturability	Reduce manufacturing time and error	Focus on simplicity and manufacturing constraints: minimize multi-planar bends; improve manufacturing capabilities







Scoundrel 87.47 lbs 66 members 120.6 ft total length of tubing

Corsair 80.69 lbs 59 members 118.7 ft total length of tubing

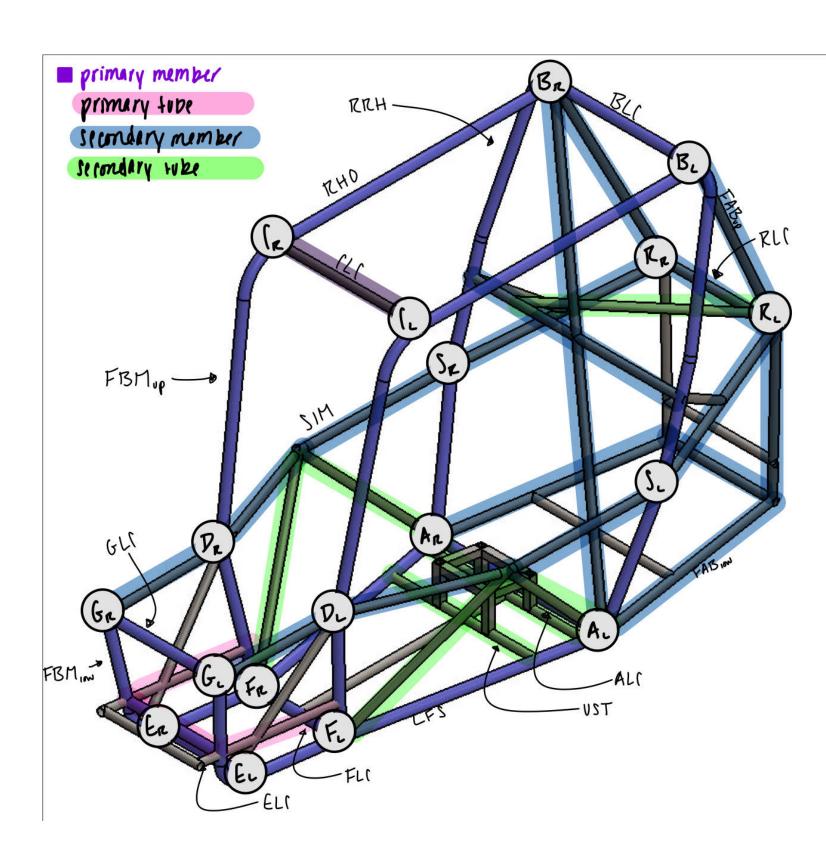
10.4% reduction in weight





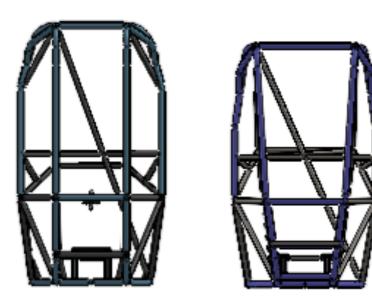


CHASSIS - Frame





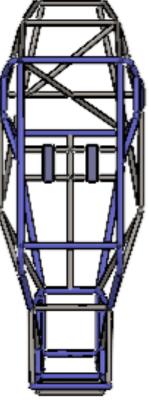
Top View: Scoundrel & Corsair

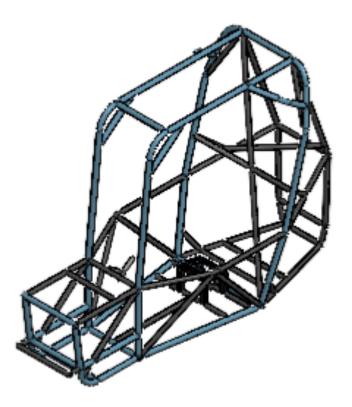


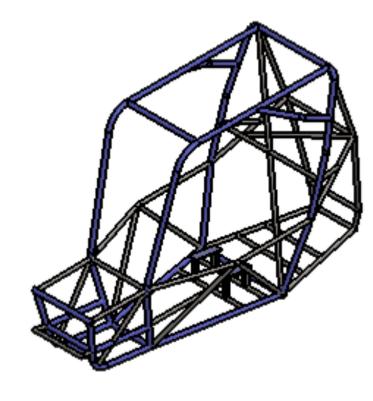
Corsair Frame w/ Named Point and Member Classification Requirements



Frame Design

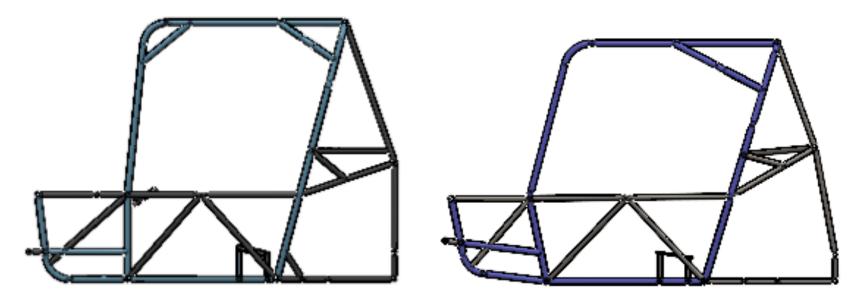






Iso View: Scoundrel & Corsair

Front View: Scoundrel & Corsair Frame Height: 56.9" --> 50.75"



Side View: Scoundrel & Corsair







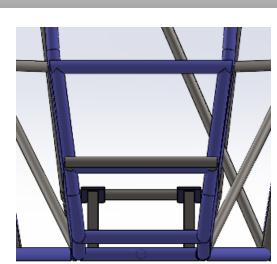


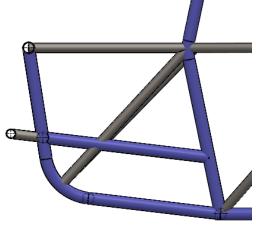




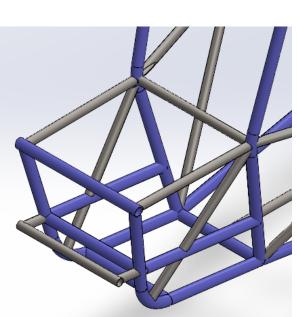
CHASSIS - Frame

Subsystem Integration

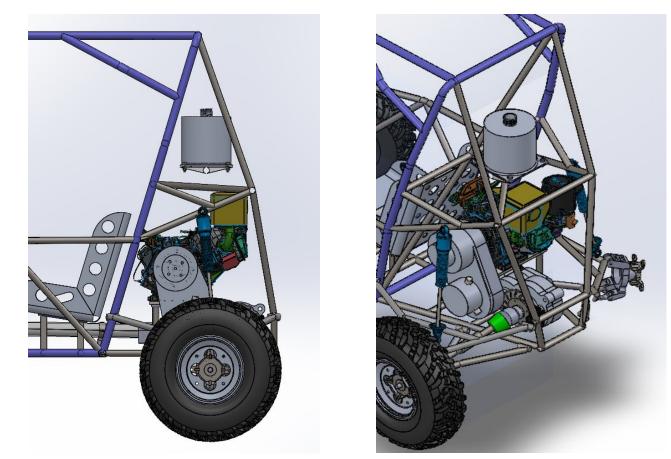




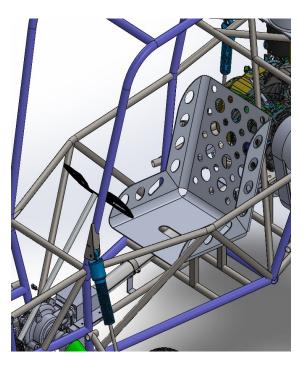
Front Suspension Rake --> Inclined and trapezoidal toebox



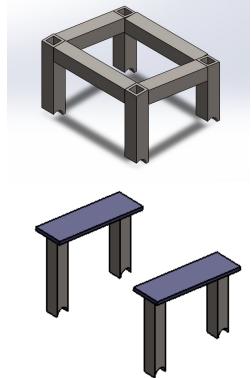




Transmission Transfer case packaging --> lengthened rear



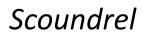




Driveline / HI Raised and angled driveshaft --> Modified seat mount









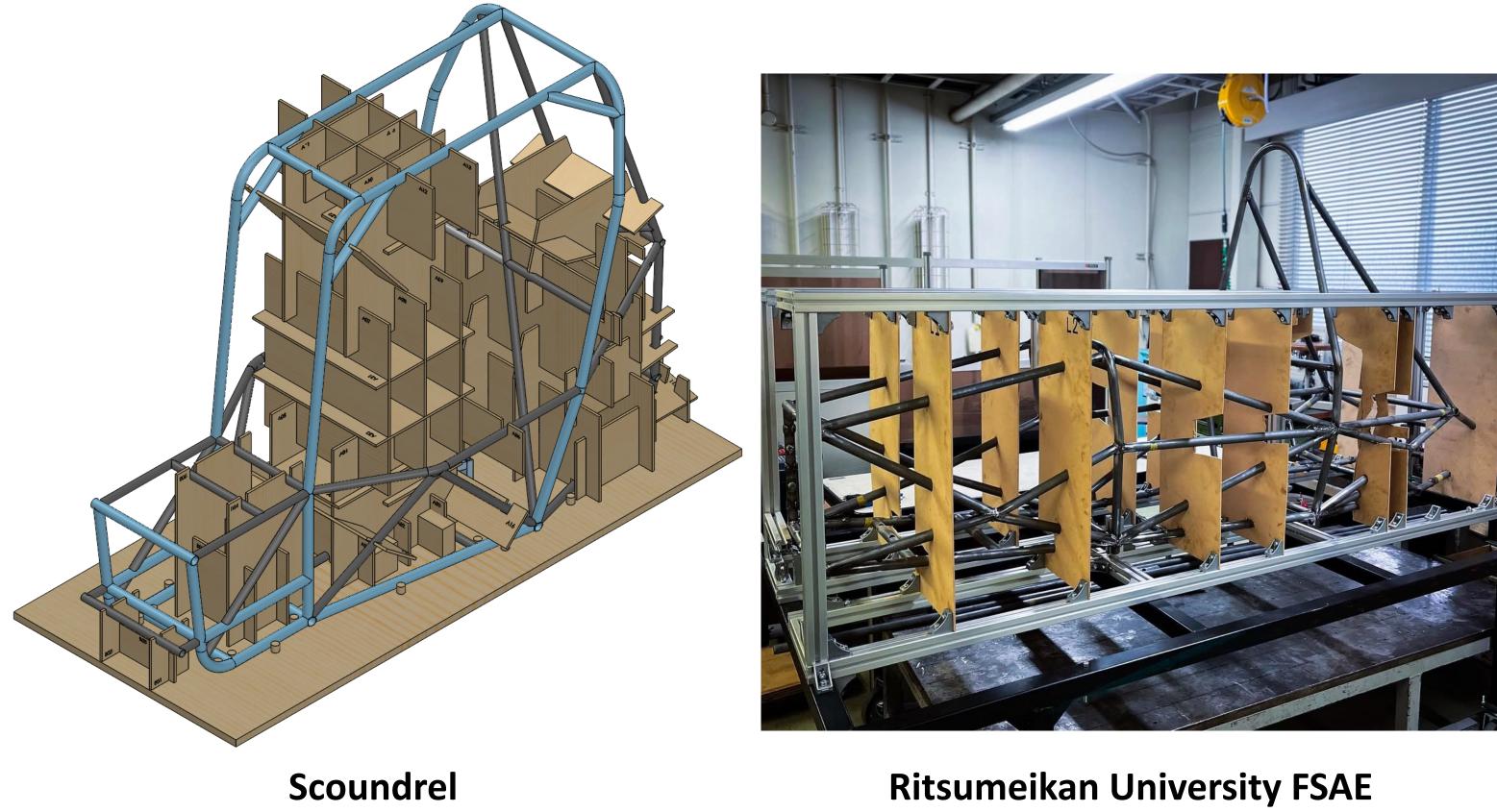




SAE INTERNATIONAL.

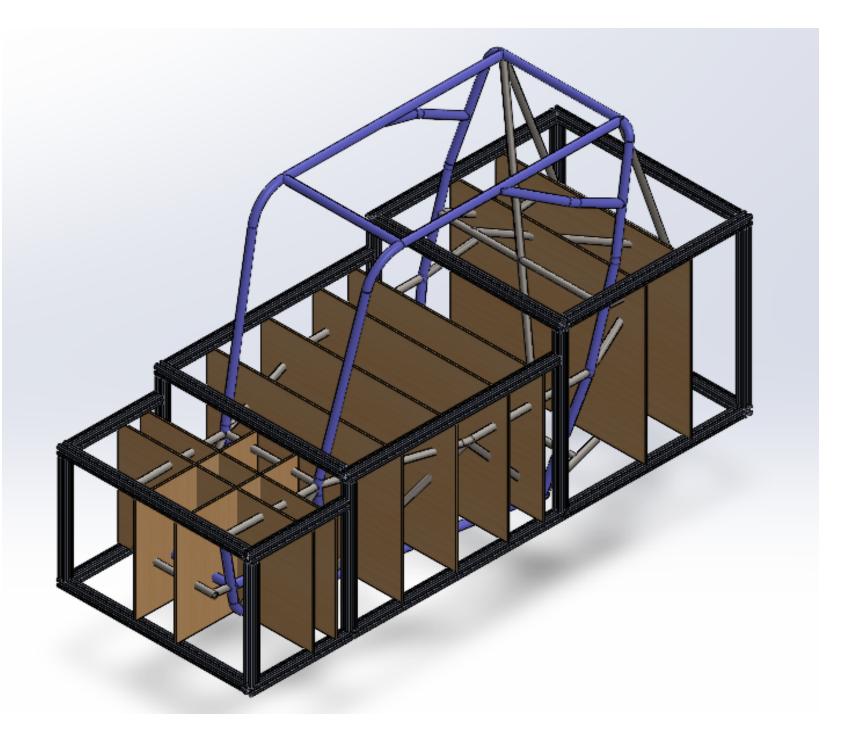
CHASSIS - Frame

Welding Jigs









Corsair Preliminary 3D Jig Idea













CHASSIS - Body

Subsystem Goals

Description	Requirement	Reason	Deliverables	"D	efinition of Success"	% Com
Weight	<11 lbs	 Scoundrel's weight = ~15.5 lbs 	Materials Justification	releva	leted technical report with all nt calculations and mech tests.	60%
Flexural Strength	TBD	 Bending Strength + Stiffness = <u>Impact</u> <u>Strength</u> 	Tooling Molds Phase 1	-	BD printed and sanded molds.	20%
Fiber-to-Resin Ratio	60:40 +/- 5%	 Measure of our manufacturing process quality and efficacy 	Manufacturing Phase 2 Preparation	• Compl	leted skidplate research/FEA and ype sandwich panel.	40%
Failure Modes	Cohesive Failure	Measure of our manufacturing process	Car Livery Design	Compl aesthe	leted conceptual design for car etic.	70%
(Sandwich Panels)		quality and efficacy	Body CAD Modeled		BD modeled racecar body and ated into master CAD.	



Fall Deliverables











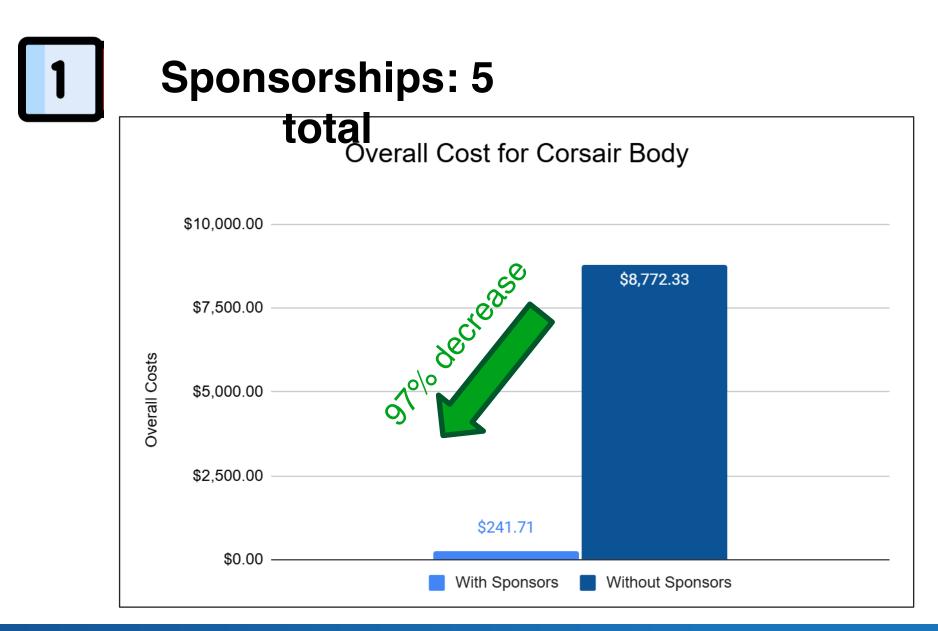




CHASSIS - Body

Cost Reduction Strategies

*Manufacturing Costs	Scoundrel – Total Costs	Corsair – Fixed Costs	Corsair – Variable Costs	Corsair – Total Costs	Overall
Body Panels	\$55.50	ሰብ አብ ማብ	\$60	\$136.97	+ 247%
Skidplate	\$251.02	\$141.71	\$40	\$104.74	- 58%
Overall	\$306.52	-	-	\$241.71	- 21%



*Nosecone and Number Panels excluded for simplicity













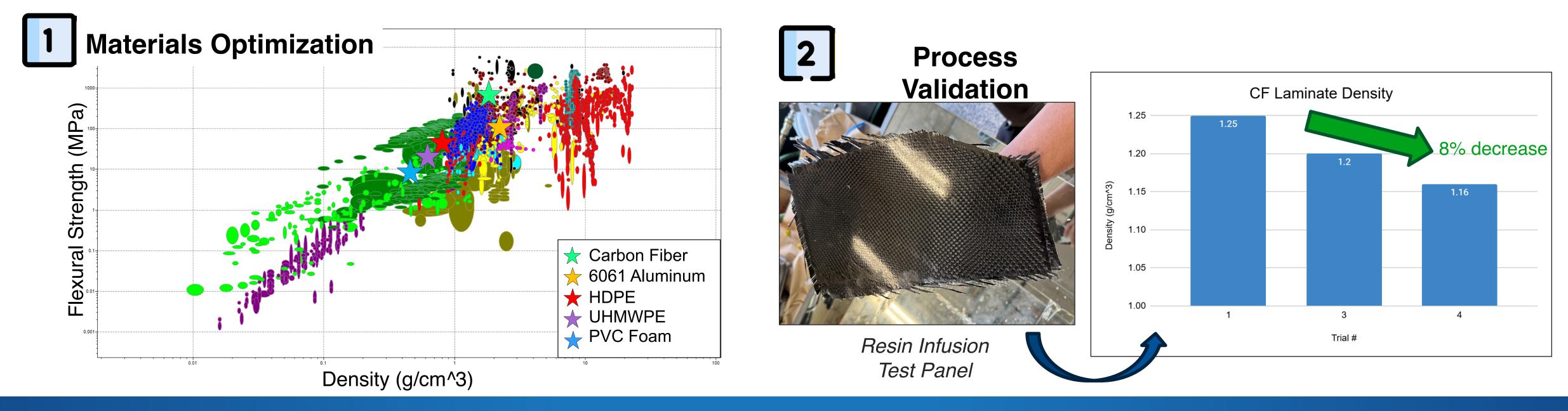




CHASSIS - Body

Weight Reduction Strategies

*Weight Reduction	Scoundrel	Materials	Corsair	Materials	% Change
Body Panels	3.59 lbs	HDPE	3.78 lbs	CF	+ 5%
Skidplate	10.78 lbs	UHMPWE / 6061 Al	6.5 lbs	CF/GF + PVC Foam Core	- 40%
Overall	14.37 lbs	-	10.28 lbs	-	- 28%



*Nosecone and Number Panels excluded for simplicity





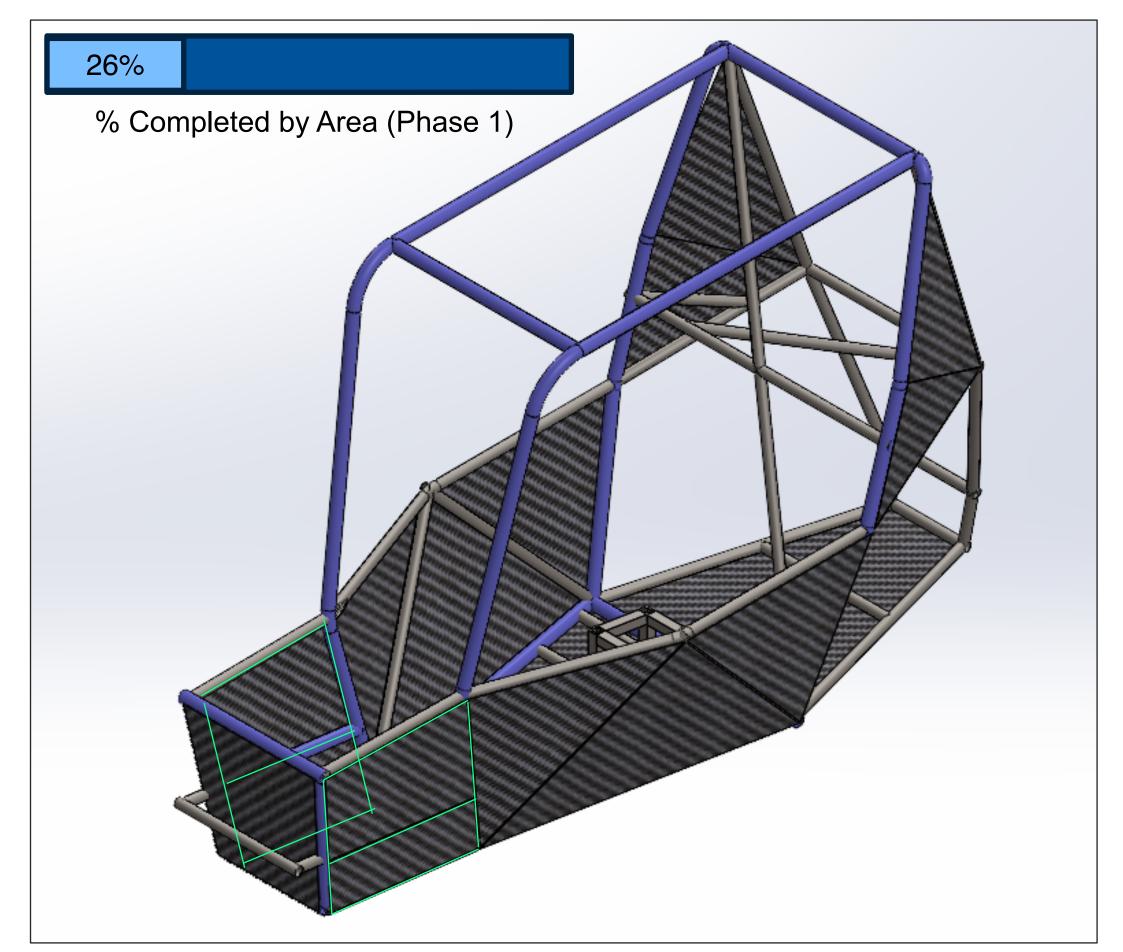






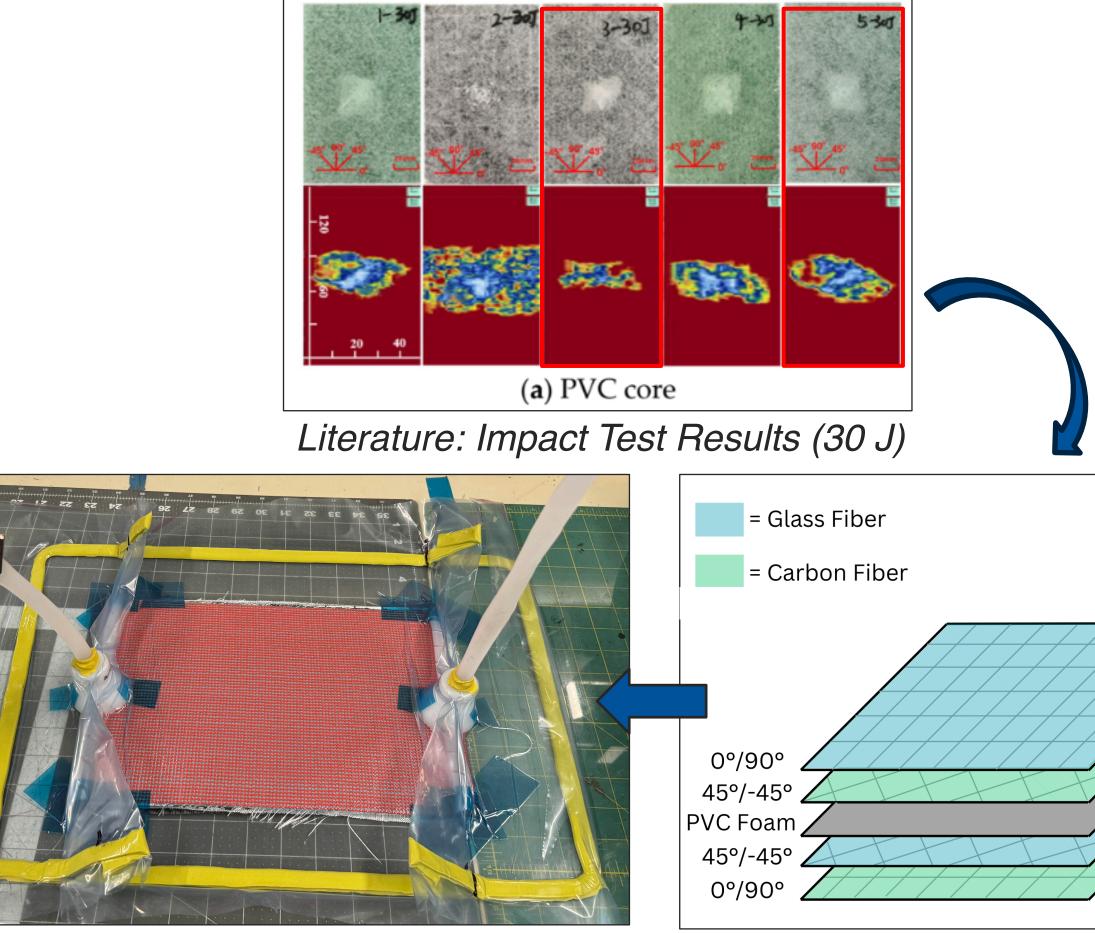
CHASSIS - Body

Manufacturing Progress



Master Body Assembly (Finished Parts in Green)





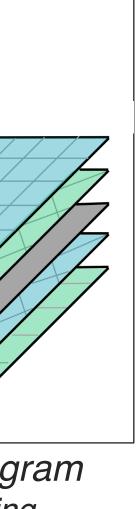
Resin Infusion of Hybrid Sandwich Panel

Laminate Stack-up Diagram Made by UCI Baja Racing

Journal of Dynamic Behavior of Materials (2018) 4:359–372 https://doi.org/10.1007/s40870-018-0163-5 Cai, Y.; Wang, X.; Ouyang, F.; Chen, Q.; Zhu, Z.; Fan, K.; Ding, F. Study on the Mechanical Properties of a Carbon-Fiber/Glass-Fiber Hybrid Foam Sandwich Structure. Materials 2024, 17, 2023. https://doi.org/10.3390/ma17092023













Goal	Reason	Plan
Weight Reduction	 Overall team goal Competitive teams had lighter cars Improved handling and acceleration 	 Cutting brake removal Smaller calipers rotors Rear inboard br
Reliability	 Lost a caliper on Rogue Kill switch failure Short brake lines on Scoundrel 	 Subsystem prototype Static and dyna testing
Driver Comfort	 Driver feedback High center of gravity 	 Implementation RAMSIS Steering wheel display Adjustable peda





System Goals rs and orake **Rotor Mount on CV Axle** amic n of T lals







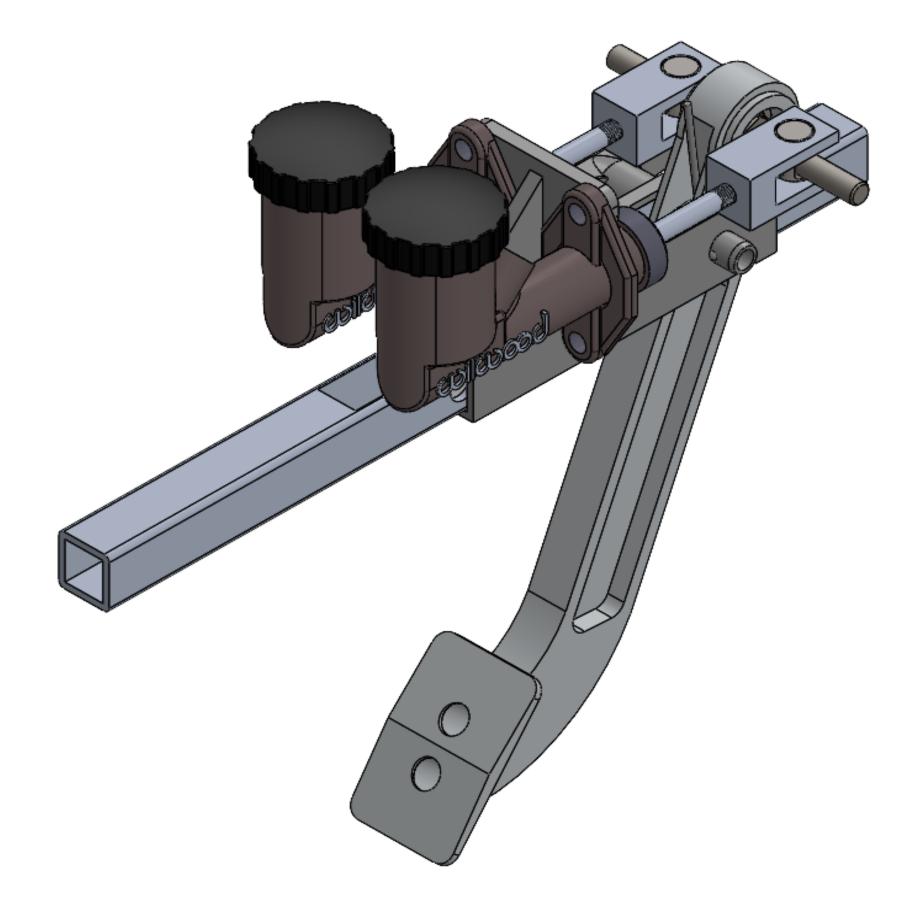








Brake Pedal Assembly



Isometric View





Scoundrel:	Corsair:
 Larger and heavier assembly (12.17 lbs) Non-adjustable Difficult to manufacture Lack of a return spring for the pedal 	 Smaller and lighter assembly (4.82 lbs) ~60% reduction in weight Two adjustable pedal positions for different drivers Easy to manufacture using square tubing Torsion spring used as return spring





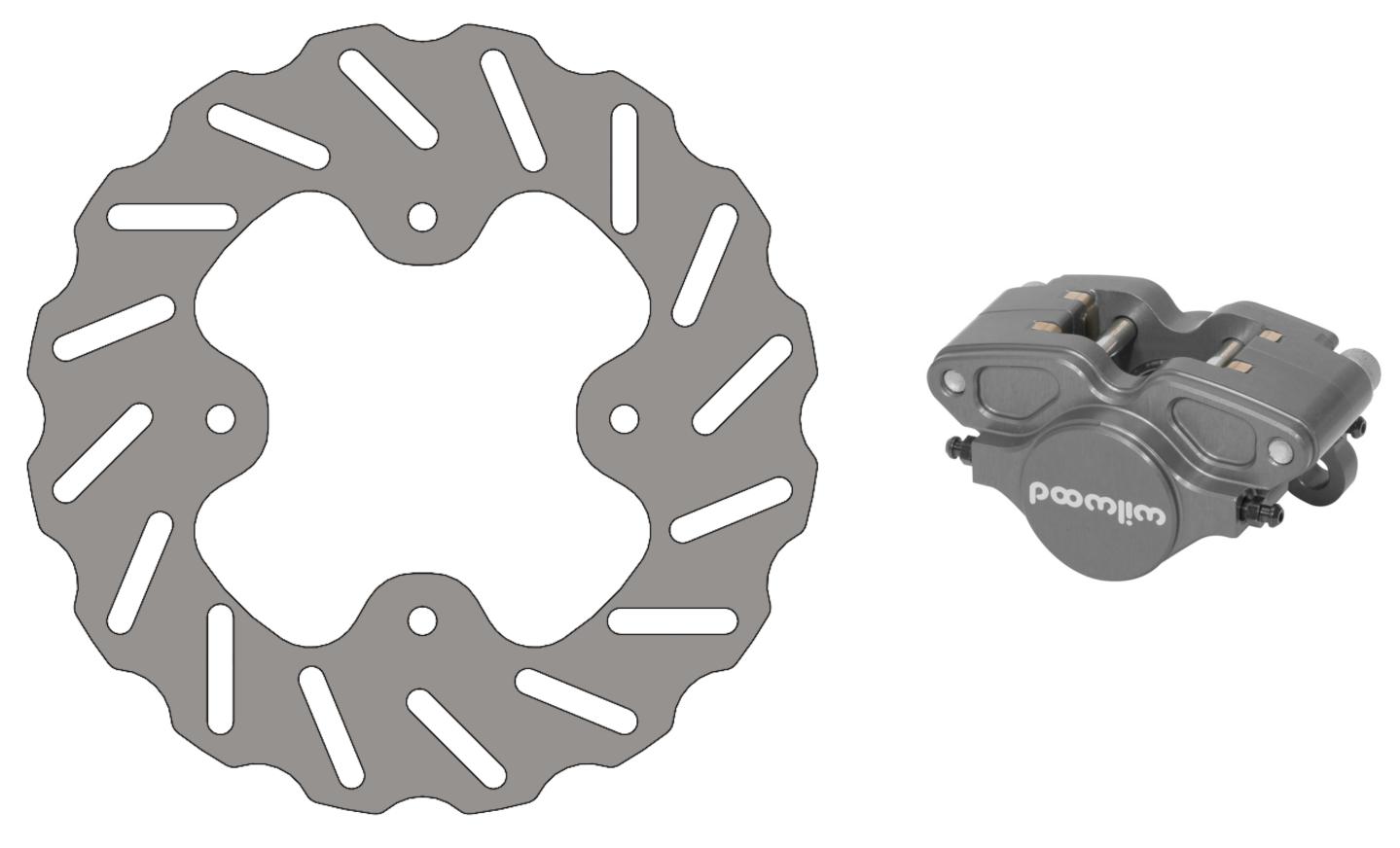












Brake Rotor





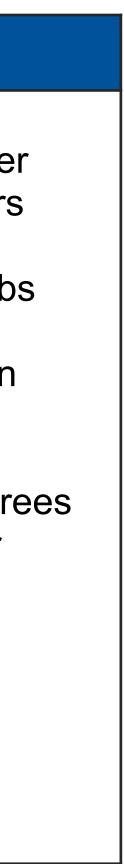
Brake Rotor

Scoundrel:	Corsair:
 Larger and heavier calipers and rotors Total weight: ~22 lbs Drilled for off-gassing Treated for corrosion resistance which is unnecessary Purchased off the shelf 	 Smaller and lighte calipers and rotors Total weight: ~8 lb ~64% reduction in weight Slotted at 45 degree and scalloped for maximum debris removal Manufacturing ourselves

Brake Caliper

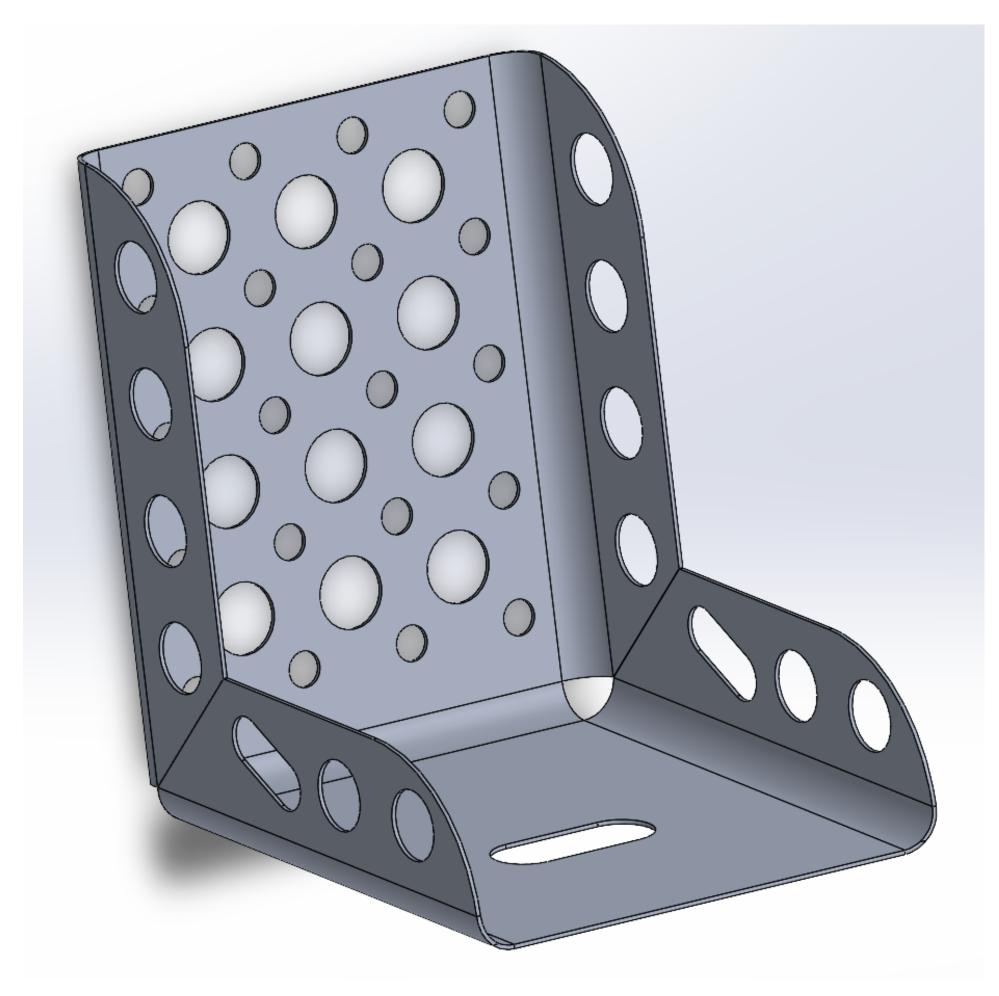












Seat





Driver Seat

Scoundrel:	Corsair:
 Seat back angle of 15 degrees Seat bottom angle of 5 degrees 	 Increased seat back angle (17 degrees) Increased seat bottom angle (9 degrees)
 Total weight: ~7 lbs No weight reduction efforts 	 Total weight: ~6 lbs ~14% reduction in weight
 Bolsters offered little to no support as they bent 	 Flanged holes for weight reduction and rigidity Large side and thigh bolsters





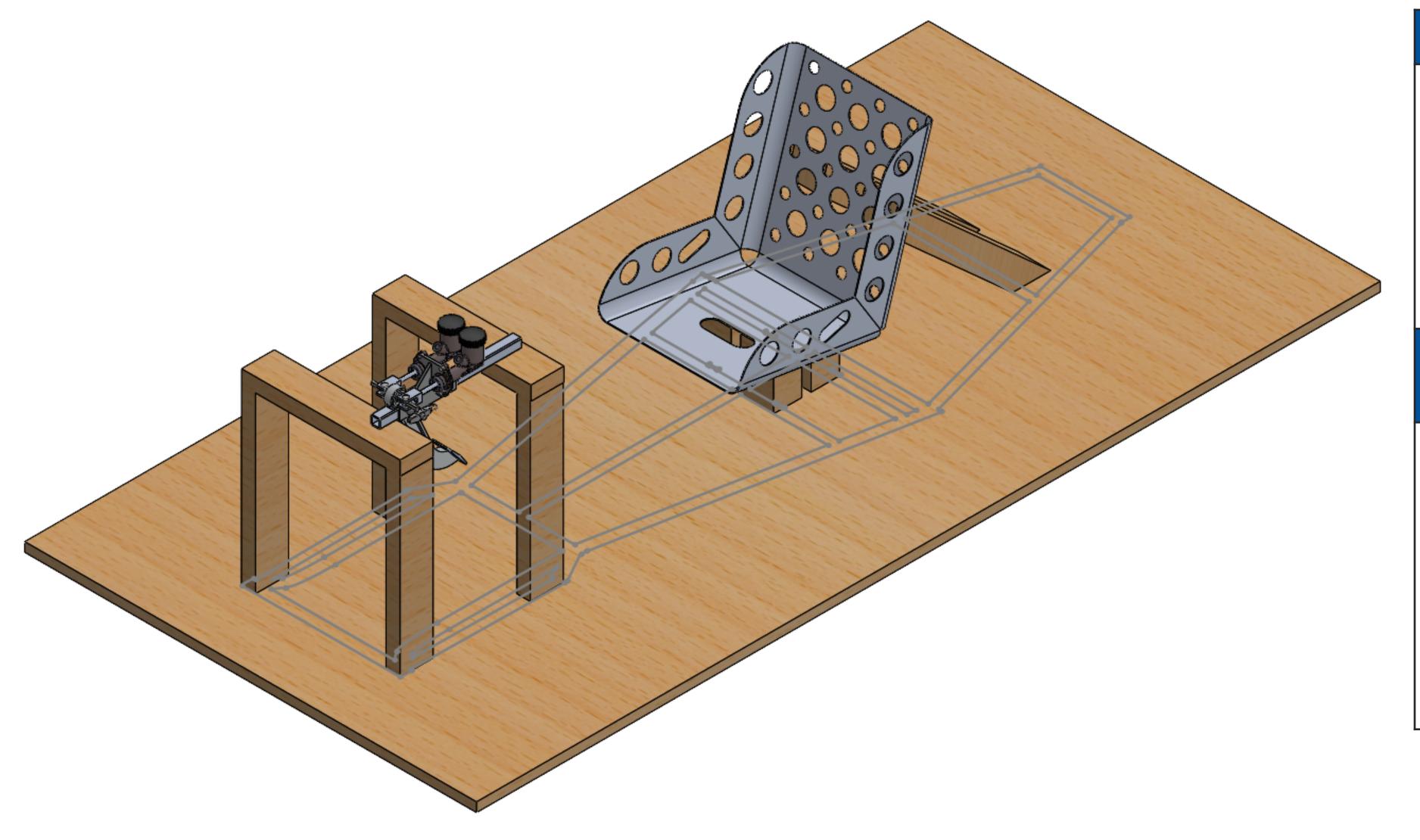








Subsystem Prototype CAD







Brakes Verification:

- Verify brake line lacksquaremanufacturing and bleeding process
- Verify calipers apply sufficient pressure to immobilize the rotor

Human Interface Verification:

- Verify driver comfort and \bullet fitment into seat
- Verify comfortable pedal distance for drivers
- Verify seat and pedal assembly rigidity











Operations and Outreach Updates

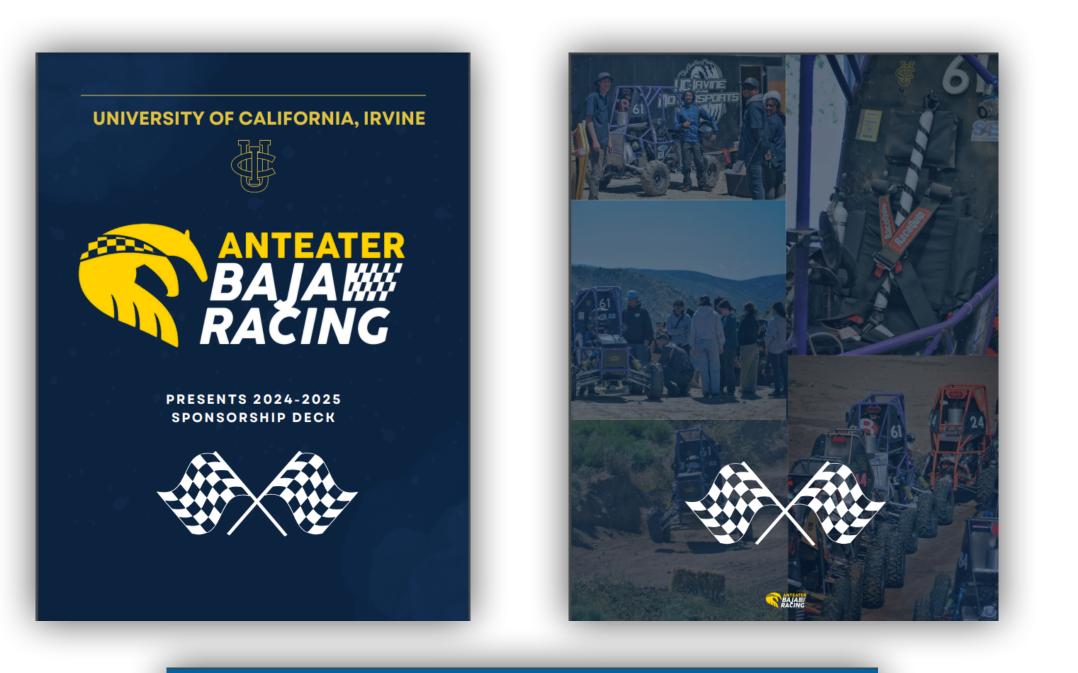
Complete:

Marketing, Logistics, and Sponsorships:

Category	Details
Sponsorships	 Connected with Sponsors. Gene Haas Foundation responded. Secured RedBull Sponsorship. ZotFunder is live.
UROP proposal	 Completed and submitted Proposal. Results : Pending
Current Website Updated	 Added full team roster. Uploaded new images. Faculty advisor page added. Home page updated.
Official Purchase Order Doc	 Standard procedure Updated format Discord reactions as updates







UCI ZotFunder

Anteater Baja Racing 2024-25











Operations and Outreach Updates

Going forward:

Comp, Logistics, and Media:

Process	Timeline	Deliverable/ Milestone
RFP : Review and Submission – official deadline	Dec 10 - Dec 13	Final RFP reviewed and approved – PMs Submit by 13th
Recruitment: Chassis and Media team	Dec 13 – Dec 15	Flyers and forms, announcements for winter recruitment
Merch: T-shirt & more	Dec 15 – Jan 5	Finalize designs, arrive early winter quarter











