

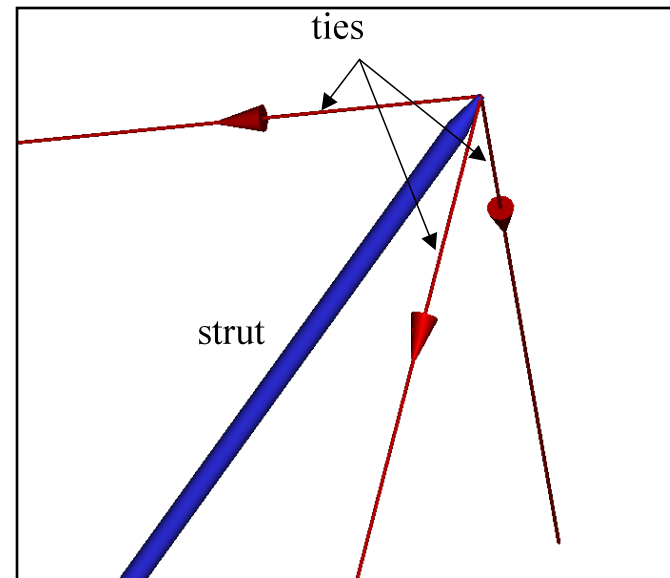
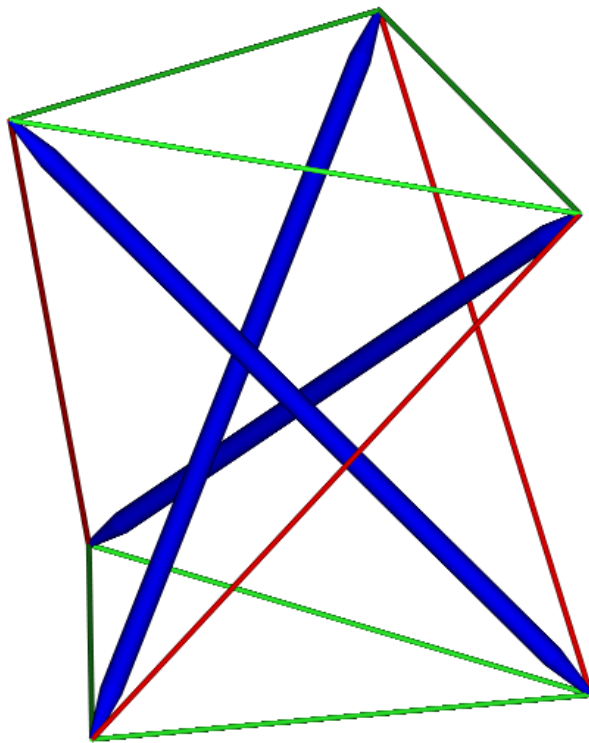
Kinestatic Analyses of Mechanisms with Compliant Elements

Carl Crane

How can such a simple mechanism have such a high order solution?

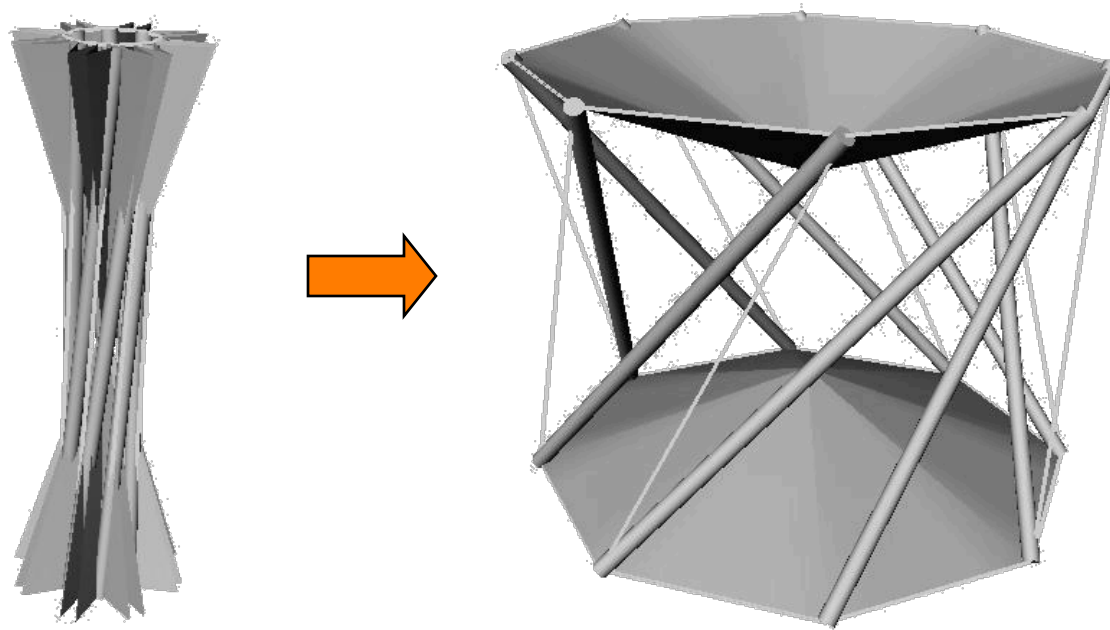
Tensegrity structures

- comprised of struts in compression and ties in tension



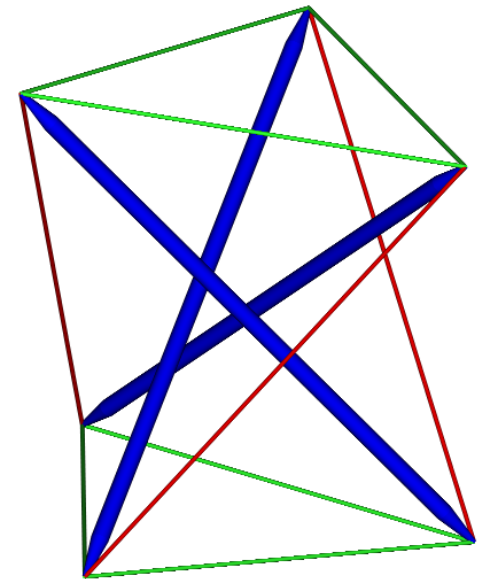
Self-deployable tensegrity structures

- certain ties replaced by elastic members



Can we solve the basic problem?

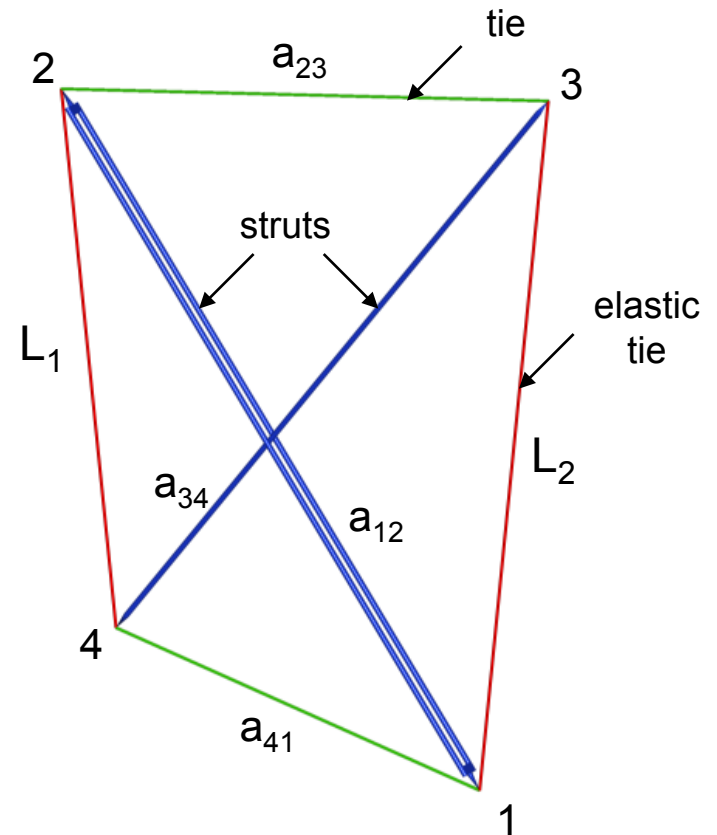
- determine in closed-form all equilibrium configurations of a self-deployable tensegrity structure given:
 - strut lengths
 - tie lengths
 - free lengths and spring constant of elastic members
 - any applied loads
- Stern [1999] performed closed-form analysis of unloaded symmetric systems
 - 2 solutions, $n=3..6$
- Correa [2001] obtained numerical solution for general loaded systems
 - numerical convergence to a solution



Let's start with a warm up problem.

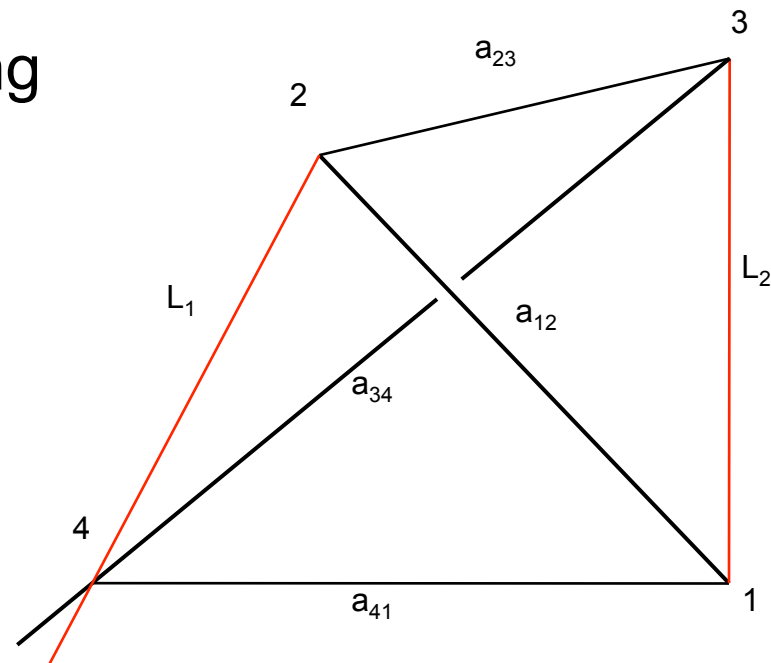
Planar 2-strut 2-spring tensegrity structure

- given:
 - strut lengths a_{12} , a_{34}
 - tie lengths a_{41} , a_{23}
 - spring parameters k_1 , L_{01} , k_2 , L_{02}
- determine:
 - all equilibrium poses



Planar 2-strut 2-spring tensegrity structure

- the struts and non-elastic ties form a simple 4-bar mechanism
- pose can be defined by one parameter
 - several descriptive parameters tried
- analysis was performed using an energy method and using L_1 as the descriptive parameter



Geometric constraints

$$A L_2^4 + B L_2^2 + C = 0$$

where

$$A = L_1^2, B = L_1^4 + B_2 L_1^2 + B_0, C = C_2 L_1^2 + C_0$$

and where

B_2 , B_0 , C_2 , and C_0 are expressed in terms of known quantities

Verification of geometric constraint equation

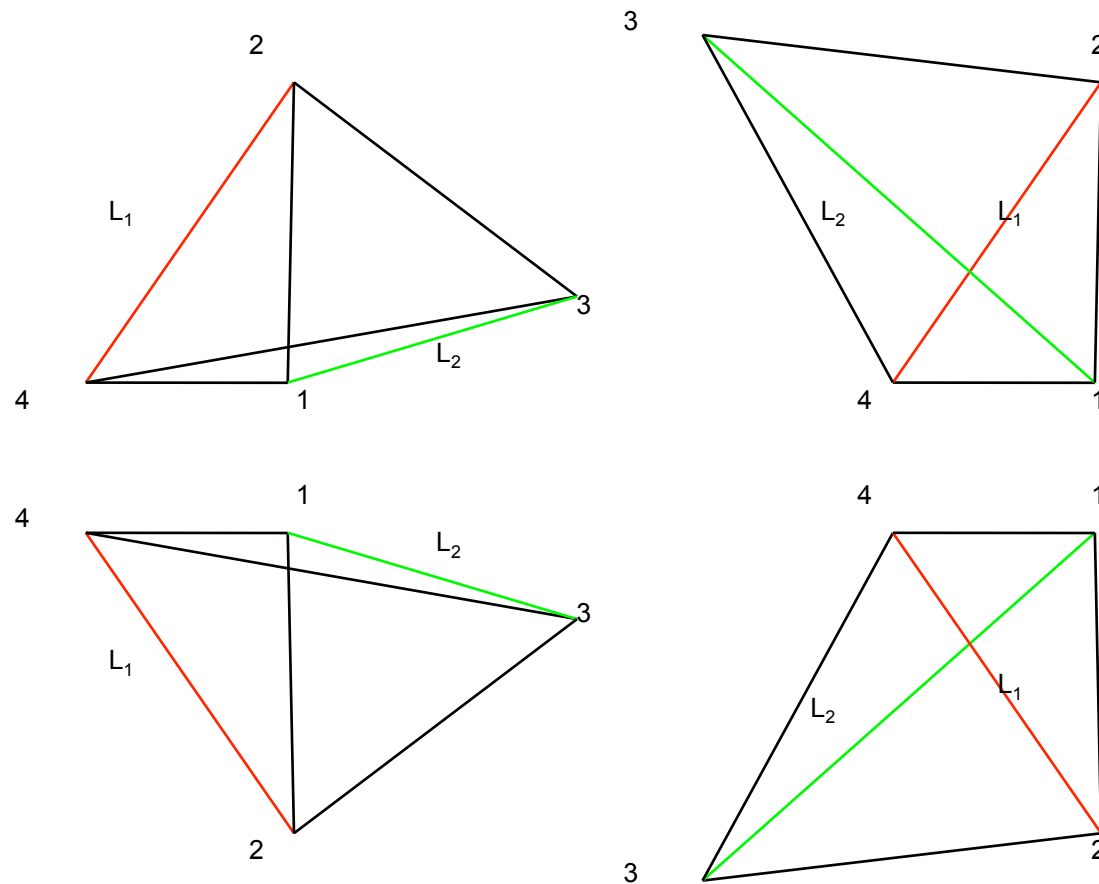


Figure 7: Possible Configurations for Numerical Example

Potential energy constraint

- at equilibrium, the potential energy in the springs will be a minimum

$$U = \frac{1}{2} k_1 (L_1 - L_{01})^2 + \frac{1}{2} k_2 (L_2 - L_{02})^2$$

- at a minimum potential energy state,

$$\frac{dU}{dL_1} = k_1 (L_1 - L_{01}) + k_2 (L_2 - L_{02}) \frac{dL_2}{dL_1} = 0 \quad (17)$$

- dL_2/dL_1 can be obtained via implicit differentiation of the geometry constraint (13) as

$$\frac{dL_2}{dL_1} = \frac{-L_1 [L_2^2 (L_2^2 + 2L_1^2 - a_{23}^2 - a_{41}^2 - a_{34}^2 - a_{12}^2) + (a_{12}^2 - a_{23}^2)(a_{41}^2 - a_{34}^2)]}{L_2 [L_1^2 (L_1^2 + 2L_2^2 - a_{23}^2 - a_{41}^2 - a_{34}^2 - a_{12}^2) + (a_{12}^2 - a_{41}^2)(a_{23}^2 - a_{34}^2)]} \quad (18)$$

Geometry and Potential energy constraints

- geometry constraint

$$A L_2^4 + B L_2^2 + C = 0 \quad (13)$$

- potential energy constraint

$$D L_2^5 + E L_2^4 + F L_2^3 + G L_2^2 + H L_2 + J = 0 \quad (19)$$

where the coefficients D through J are polynomials in L_1

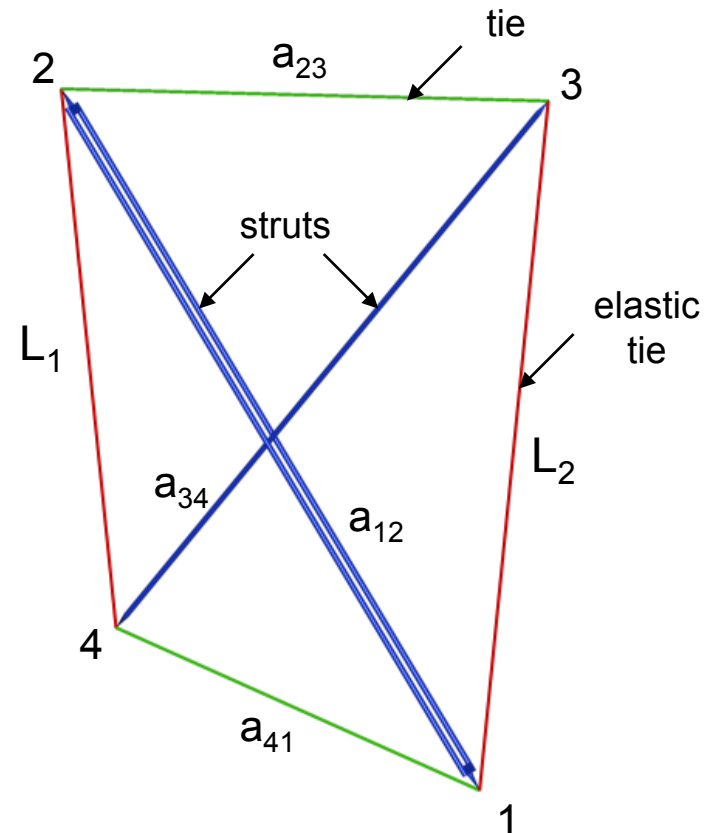
- Sylvester's elimination method can be used to identify the condition that the coefficients must satisfy in order for (13) and (19) to have common roots for L_2
 - multiply (13) by L_2, L_2^2, L_2^3, L_2^4
 - multiply (19) by L_2, L_2^2, L_2^3

– obtain 9 'homogeneous' equations in 9 unknowns

Sylvester's elimination

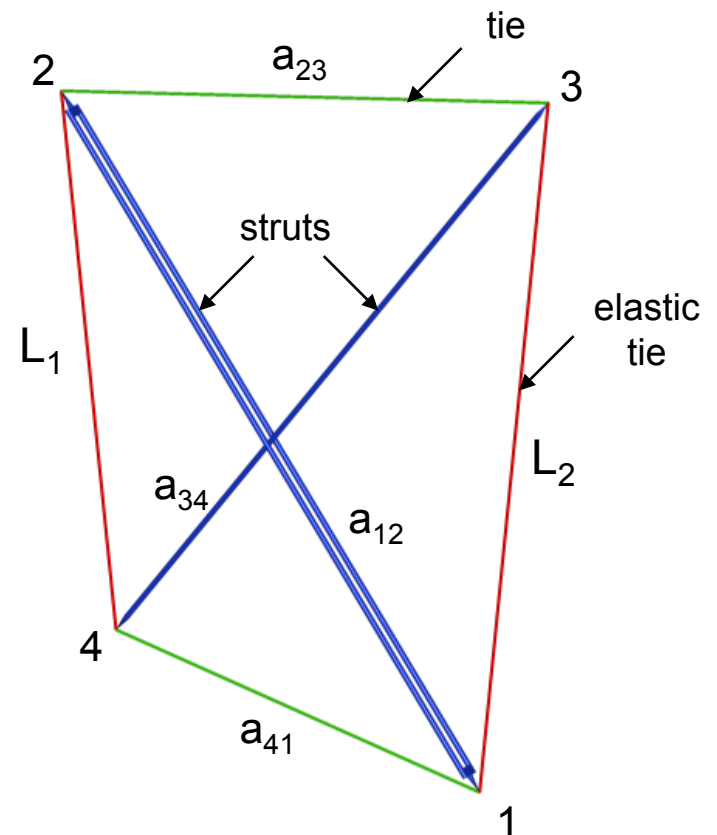
$$\begin{bmatrix} 0 & 0 & 0 & D & E & F & G & H & J \\ 0 & 0 & 0 & 0 & A & 0 & B & 0 & C \\ 0 & 0 & 0 & A & 0 & B & 0 & C & 0 \\ 0 & 0 & D & E & F & G & H & J & 0 \\ 0 & 0 & A & 0 & B & 0 & C & 0 & 0 \\ 0 & D & E & F & G & H & J & 0 & 0 \\ 0 & A & 0 & B & 0 & C & 0 & 0 & 0 \\ D & E & F & G & H & J & 0 & 0 & 0 \\ A & 0 & B & 0 & C & 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} L_2^8 \\ L_2^7 \\ L_2^6 \\ L_2^5 \\ L_2^4 \\ L_2^3 \\ L_2^2 \\ L_2 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

- determinant of coefficient matrix must equal zero which yields a **28th degree polynomial** in L_1



Numerical example

- given:
 - $a_{12} = 3$ in. $a_{34} = 3.5$ in.
 - $a_{41} = 4$ in. $a_{23} = 2$ in.
 - $L_{01} = 0.5$ in. $k_1 = 4$ lbf/in.
 - $L_{02} = 1$ in. $k_2 = 2.5$ lbf/in.
- find L_1 and L_2 at equilibrium

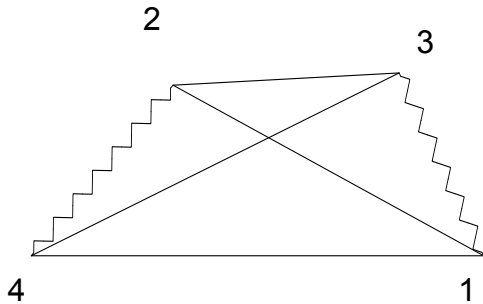


Numerical Example

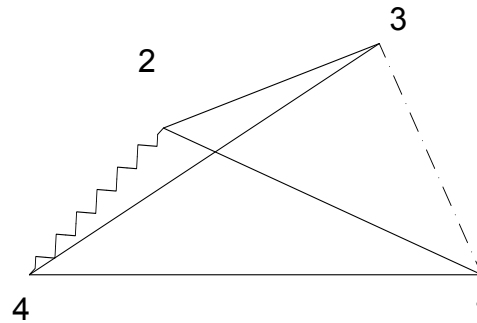
- results
 - coefficients of 28th degree polynomial in L_1 obtained
 - 8 real roots for L_1 with corresponding values for L_2
 - all 20 complex solution pairs (L_1, L_2) satisfied equations (13) and (19), i.e. geometry constraint and $dU/dL_1 = 0$
 - 4 cases correspond to minimum potential energy

Case	L_1 , in.	L_2 , in.
1	-5.4854	2.3333
2	-5.3222	-2.9009
3	-1.7406	-1.4952
4	-1.5760	1.8699
5	1.6280	1.7089
6	1.8628	-1.3544
7	5.1289	-3.2880
8	5.4759	2.3938

Numerical Example

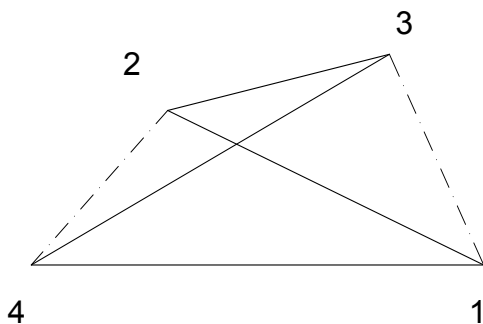


Case 3

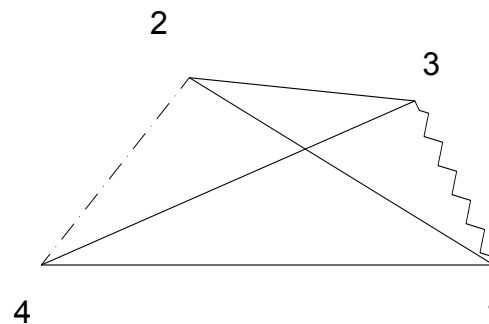


Case 4

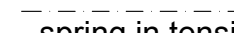
 spring in compression with a negative spring length



Case 5

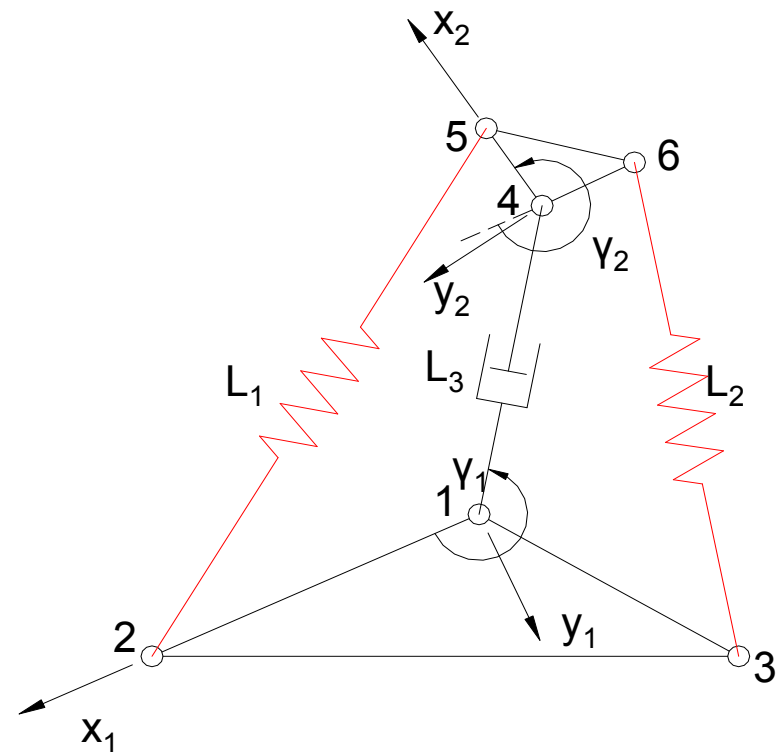


Case 6

 spring in tension

Let's look at a second simple problem.

- In many papers involving compliant elements, researchers assume that their springs have a free length of zero.
- How much more complicated does the problem become if the spring free lengths are not zero?



Problem Statement

- given:

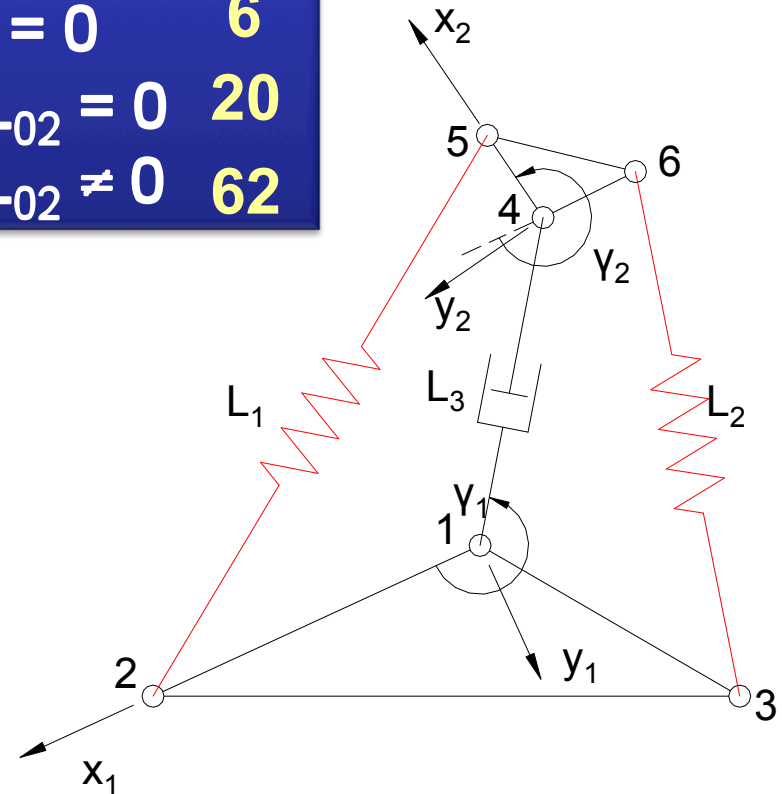
- L_{12} , p_{3x} , p_{3y}
- L_{45} , p_{6x} , p_{6y}
- L_3
- k_1 , L_{01}
- k_2 , L_{02}

3 cases

1. $L_{01} = L_{02} = 0$ 6
2. $L_{01} \neq 0, L_{02} = 0$ 20
3. $L_{01} \neq 0, L_{02} \neq 0$ 62

- find:

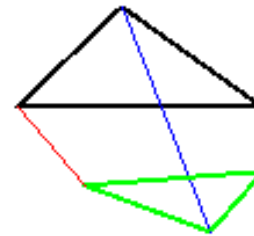
- γ_1 and γ_2 for all equilibrium configurations



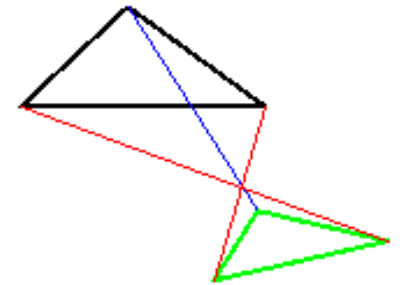
Case 1: Numerical Example

$L_{12} = 6 \text{ m}$,
 $p_{3x} = -1.25 \text{ m}$, $p_{3y} = 6.887489 \text{ m}$,
 $L_{45} = 5.5 \text{ m}$,
 $p_{6x} = -1.14 \text{ m}$, $p_{6y} = -3.13 \text{ m}$
 $L_3 = 10 \text{ m}$
 $k_1 = 2 \text{ N/m}$, $L_{01} = 0$,
 $k_2 = 3.5 \text{ N/m}$, $L_{02} = 0$

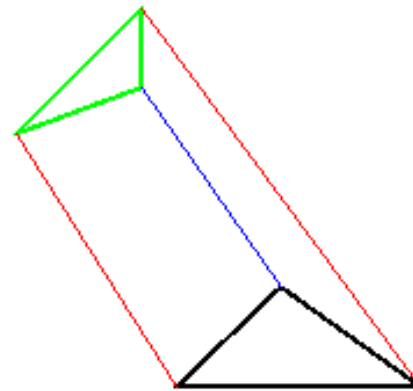
Solution #	γ_1 , radians	γ_2 , radians
1	1.1787	-1.1286
2	1.3704	2.1649
3	-1.7201	-0.4096
4	-2.0088	2.3924
5	-2.7032 + 1.1498 i	-2.6012 + 2.9712 i
6	-2.7032 - 1.1498 i	-2.6012 - 2.9712 i



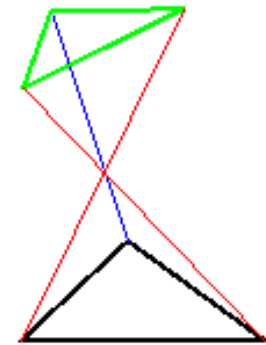
case 1



case 2



case 3



case 4

Case 2: $L_{02} = 0, L_{01} \neq 0$

$$(E_1 x_2^2 + E_2 x_2 + E_3) d_1 + E_4 x_2^2 + E_5 x_2 + E_6 = 0$$

$$(F_1 x_2^2 + F_2 x_2 + F_3) d_1 + F_4 x_2^2 + F_5 x_2 + F_6 = 0$$

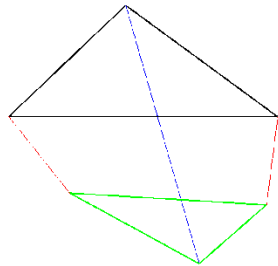
$$(G_1 x_2^2 + G_2 x_2 + G_3) d_1^2 + G_4 x_2^2 + G_5 x_2 + G_6 = 0$$

- Sylvester's Solution method
 - First two equations are multiplied by x_2 , d_1 , and $d_1 x_2$, d_1^2 and $d_1^2 x_2$. Third equation multiplied by x_2 , d_1 , and $d_1 x_2$.
 - Results in 16 'homogeneous' equations in 16 unknowns.
 - The determinant of the coefficient matrix must equal zero.
 - Resulted in a 32nd degree polynomial in x_1 .
 - Divided by $(1+x_1^2)^4$ and by square of the 2nd degree polynomial corresponding to $d_2 = 0$.

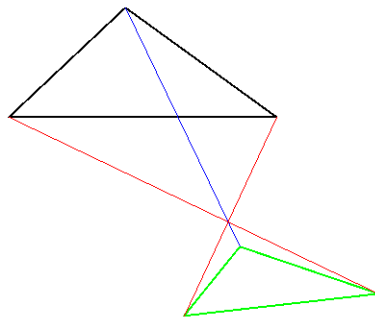
20th degree solution

Case 2: Numerical Example

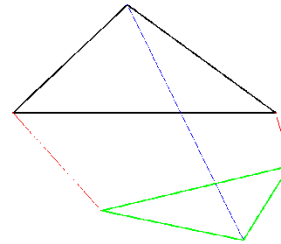
- $L_{01} = 2.3$ m, 8 real solutions



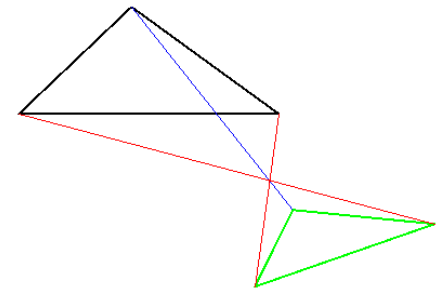
case 1



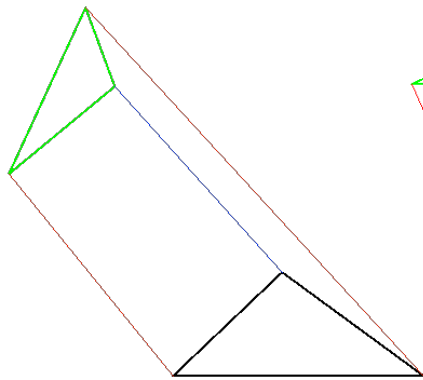
case 2



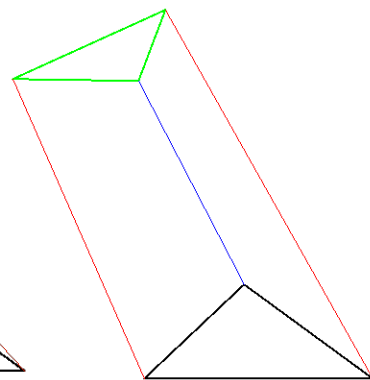
case 3



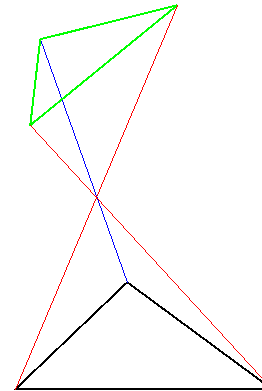
case 4



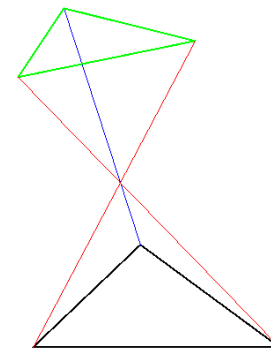
case 5



case 6



case 7



case 8

Case 3: $L_{02} \neq 0, L_{01} \neq 0$

- Will obtain 4 equations of the form

$$(C_1 x_2^2 + C_2 x_2 + C_3) + (C_4 x_2^2 + C_5 x_2 + C_6) d_{2i} + (C_7 x_2^2 + C_8 x_2 + C_9) d_{1i} = 0 \quad (1)$$

$$(D_1 x_2^2 + D_2 x_2 + D_3) + (D_4 x_2^2 + D_5 x_2 + D_6) d_{2i} + (D_7 x_2^2 + D_8 x_2 + D_9) d_{1i} = 0 \quad (2)$$

$$(M_1 x_2^2 + M_2 x_2 + M_3) + (M_4 x_2^2 + M_5 x_2 + M_6) d_{1i}^2 = 0 \quad (3)$$

$$(N_1 x_2^2 + N_2 x_2 + N_3) + (N_4 x_2^2 + N_5 x_2 + N_6) d_{2i}^2 = 0 \quad (4)$$

where the coefficients are functions of x_1

Case 3: $L_{02} \neq 0, L_{01} \neq 0$

- Multiply Equations (1), (2) by
 - $\{1, d_{1i}, d_{2i}, d_{1i}^2, d_{2i}^2, d_{1i}d_{2i}, d_{1i}^2d_{2i}, d_{1i}d_{2i}^2\} * \{1, x_2\}$
- Multiply Equation (3) by
 - $\{1, d_{1i}, d_{2i}, d_{1i}d_{2i}, d_{2i}^2\} * \{1, x_2\}$
- Multiply Equation (4) by
 - $\{1, d_{1i}, d_{2i}, d_{1i}d_{2i}, d_{1i}^2\} * \{1, x_2\}$
- Total Equations = 52
- Unknowns
 - $\{1, d_{1i}, d_{2i}, d_{1i}^2, d_{2i}^2, d_{1i}d_{2i}, d_{1i}^2d_{2i}, d_{1i}d_{2i}^2, d_{1i}^3, d_{2i}^3, d_{1i}^3d_{2i}, d_{1i}d_{2i}^3, d_{1i}d_{2i}^3\} * \{x_2^3, x_2^2, x_2, 1\}$

Case 3: $L_{02} \neq 0, L_{01} \neq 0$

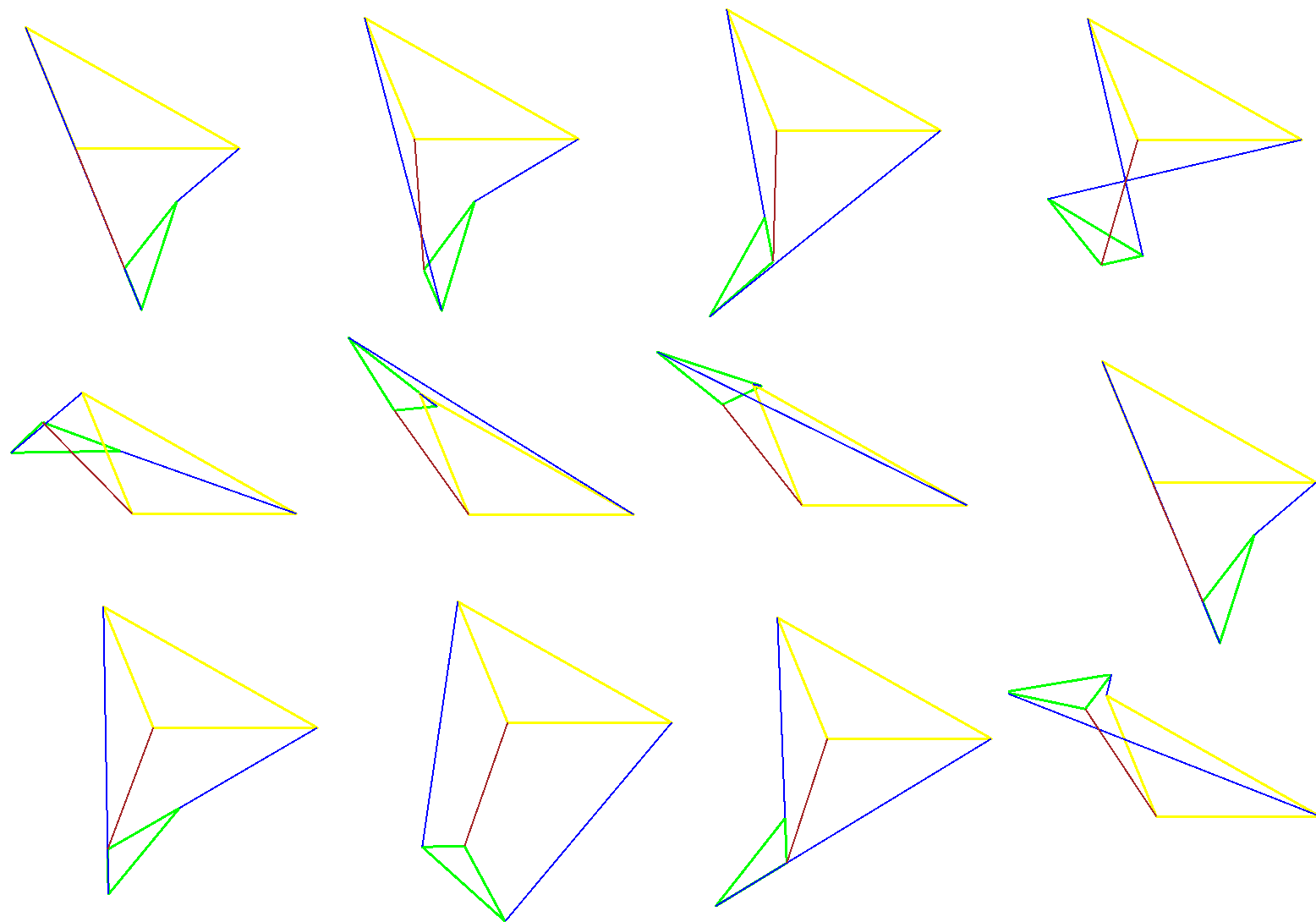
- Expansion of $|\mathbf{M}| = 0$ yielded a 104th degree polynomial in x_1 .
- This can be divided by $(1+x_1^2)^{13}$ to get 78th degree polynomial in x_1 .
- Of the 78 solutions 16 were extraneous.
- 62 solutions were obtained.
- Numerical continuation method* found 88 solutions (62 + 26 circular points).

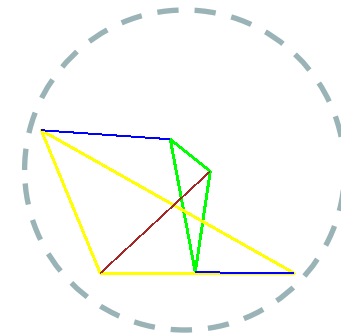
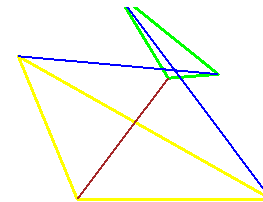
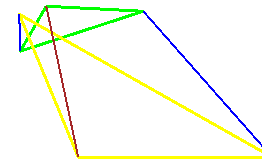
* *PHCpack software, Jan Verschelde, U. Illinois, Chicago*

Case 3: $L_{02} \neq 0$, $L_{01} \neq 0$

- $L_{01} = 5.1$ m, $L_{02} = 6.6309$ m
- Out of the 62 solutions – 38 were complex and 24 were real
- All the solutions satisfy the four equations

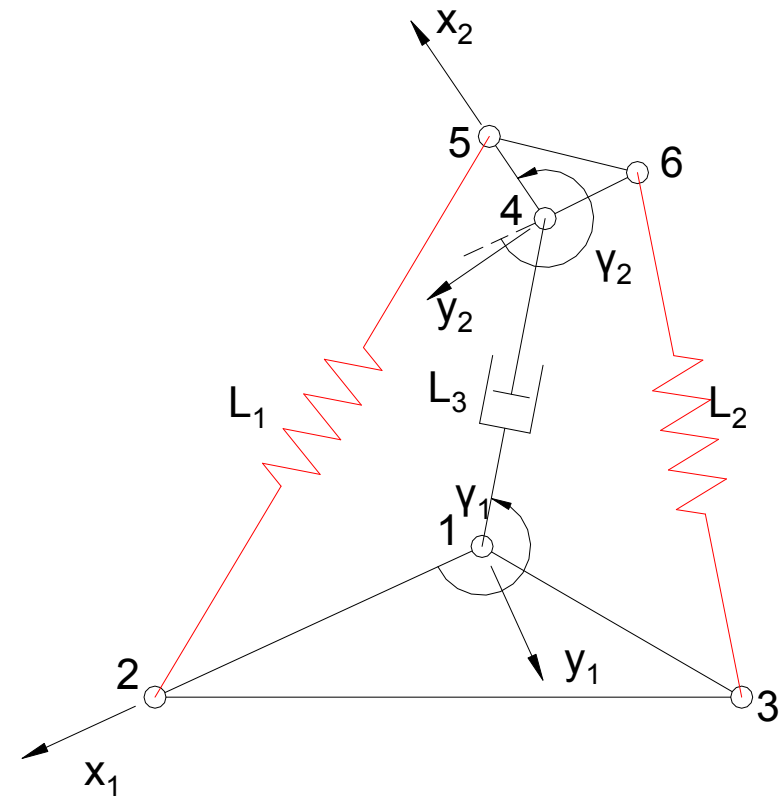
Case 3: Real Solutions - I





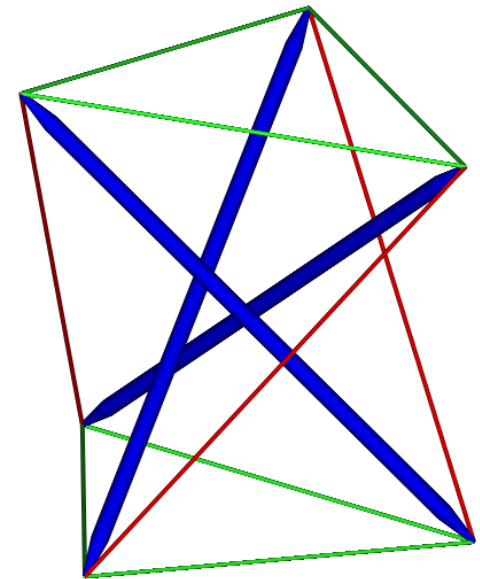
Conclusion

- Case 1, $L_{01} = L_{02} = 0$
 - 6 solutions
- Case 2: $L_{02} = 0, L_{01} \neq 0$
 - 20 solutions
- Case 3: $L_{02} \neq 0, L_{01} \neq 0$
 - 62 solutions

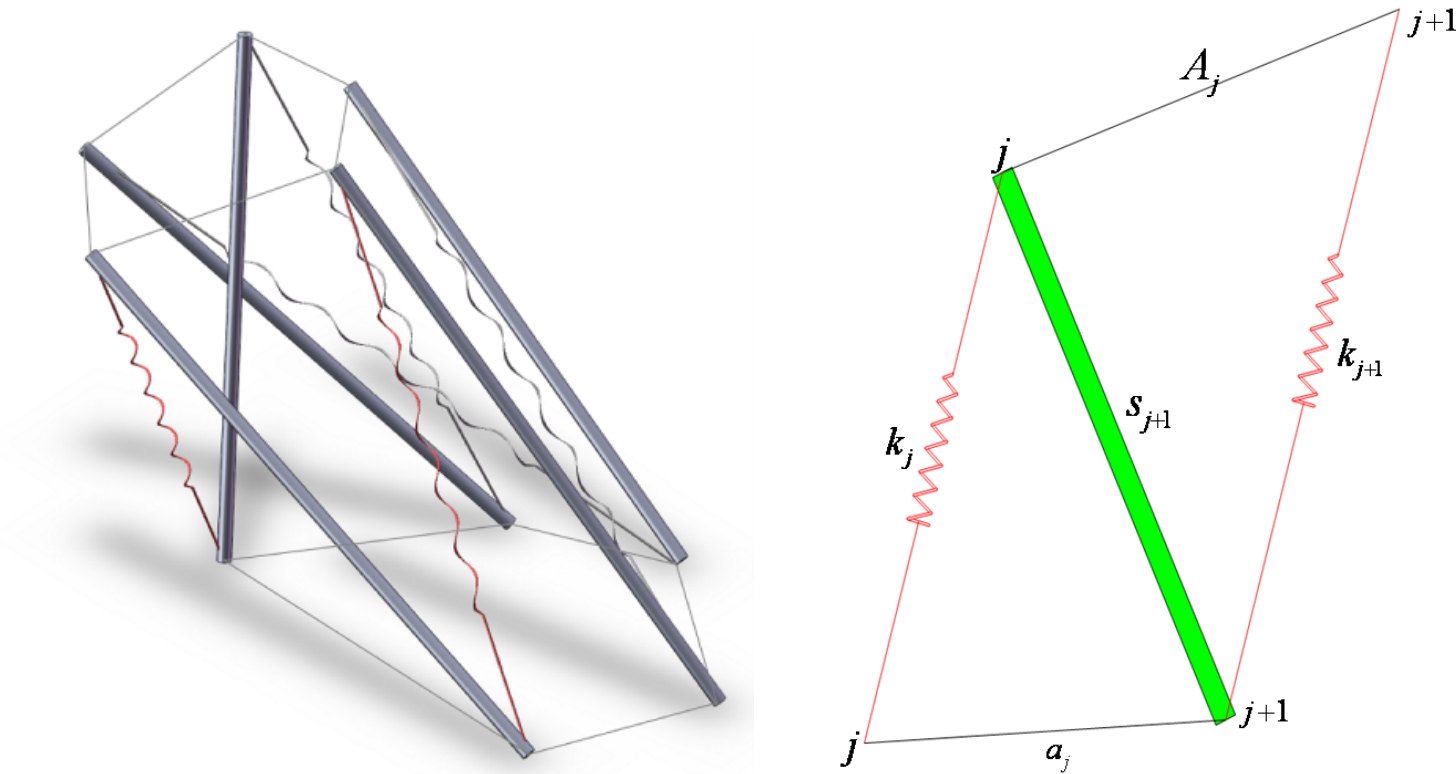


Back to the primary problem.

- given:
 - strut lengths
 - top tie lengths
 - bottom tie lengths
 - spring constant and free length of side ties
- find:
 - all equilibrium configurations



How to structure the problem?



First, attempt to solve the problem when all the spring free lengths equal zero.

Problem Formulation

- given: A_j, a_j, k_j
- find: $X_j, Y_j, Z_j, x_j, y_j, z_j$
such that

$$u = \frac{1}{2} \sum_{j=1}^n \left(\left(\begin{matrix} X_j \\ Y_j \\ Z_j \end{matrix} \right)^T \begin{pmatrix} a_j \\ 0 \\ 0 \end{pmatrix} - \frac{1}{2} \left(\begin{matrix} X_j \\ Y_j \\ Z_j \end{matrix} \right)^T \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} \right)$$

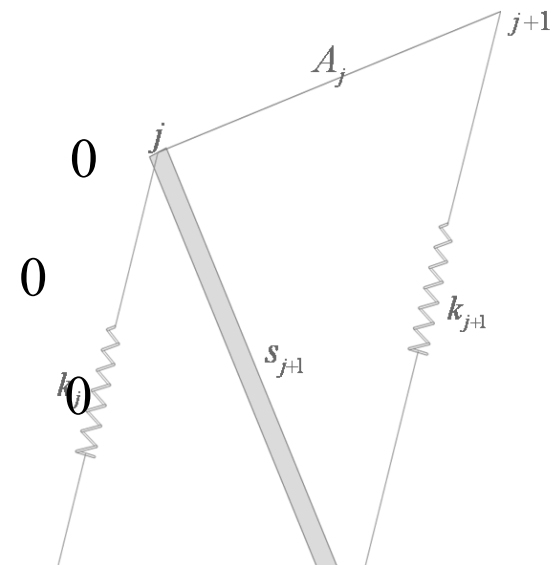
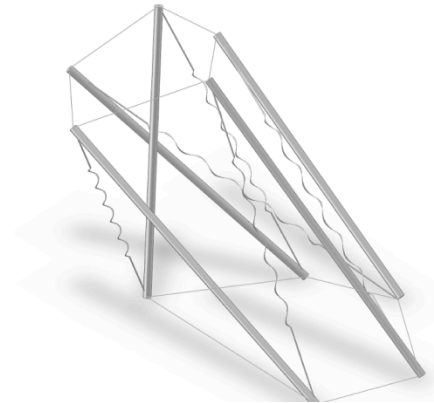
is an extremum subject to

$$g_1(X_j, Y_j, Z_j) = \left(\begin{matrix} X_j \\ Y_j \\ Z_j \end{matrix} \right)^T \begin{pmatrix} a_j \\ 0 \\ 0 \end{pmatrix} - \frac{1}{2} \left(\begin{matrix} X_j \\ Y_j \\ Z_j \end{matrix} \right)^T \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} = 0$$

$$g_2(X_j, Y_j, Z_j) = \left(\begin{matrix} X_j \\ Y_j \\ Z_j \end{matrix} \right)^T \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} - \frac{1}{2} \left(\begin{matrix} X_j \\ Y_j \\ Z_j \end{matrix} \right)^T \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} = 0$$

$$g_3(X_j, Y_j, Z_j) = \left(\begin{matrix} X_j \\ Y_j \\ Z_j \end{matrix} \right)^T \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} - \frac{1}{2} \left(\begin{matrix} X_j \\ Y_j \\ Z_j \end{matrix} \right)^T \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} = 0$$

for $j = 1 \dots n$.



This formulation was selected to avoid any need to use tan half-angle substitutions to convert trigonometric functions into polynomials.

Example

Three strut tensegrity where spring free lengths equal zero.

There are 9 unknowns, i.e. $X_j, Y_j, Z_j, j=1..3$.

There are 9 constraint equations:

$$k k_{\Delta \Delta}^{22} + = 0$$

$$k_2 k_3 \Delta_{23}^2 \Delta_{32}^2 + = | \quad || \quad | \quad 0$$

$$kk_{33}|\Delta_{1113}^{22}|\Delta\Delta|+=|||0$$

[illegible]

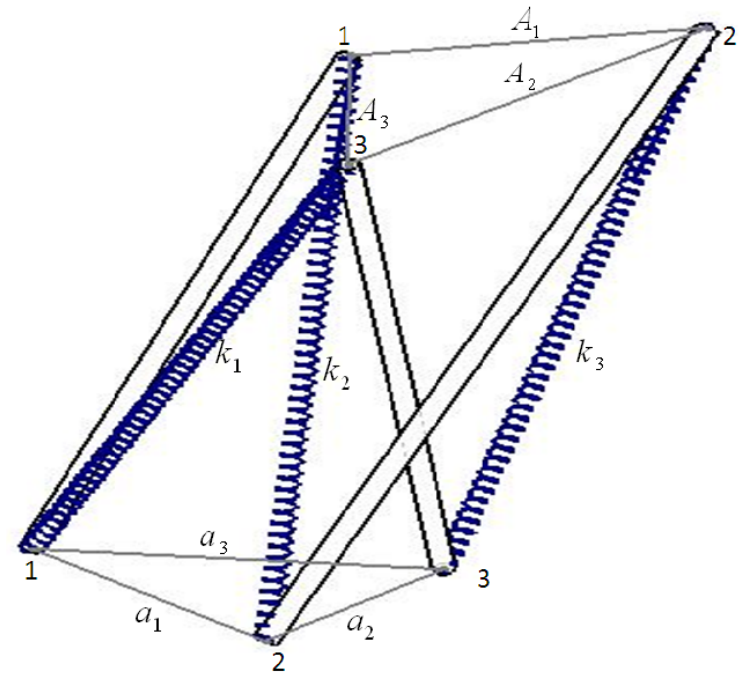
$$(X_{1212122})^{222} = \begin{pmatrix} & & \\ & & \\ & & \end{pmatrix} \begin{pmatrix} & & \\ & & \\ & & \end{pmatrix}^2 = 0$$

$$\begin{pmatrix} XX & XX & XX \\ 22 & 22 & 22 \\ 22 & 22 & 22 \end{pmatrix} = \begin{pmatrix} \quad & \quad & \quad \\ \quad & \quad & \quad \\ \quad & \quad & \quad \end{pmatrix} \begin{pmatrix} \quad & \quad & \quad \\ \quad & \quad & \quad \\ \quad & \quad & \quad \end{pmatrix}^2 = 0$$

$$(X_{\mathbb{Z}_3}, \mathbb{Z}_3, \mathbb{Z}_3) \stackrel{222}{=} \left(\begin{pmatrix} & \\ & \end{pmatrix} \right) \left(\begin{pmatrix} & \\ & \end{pmatrix} \right)^2 = 0$$

$$(X_{1313135}^{222})_{24} \left(\begin{array}{c} \\ \\ \\ \end{array} \right) \left(\begin{array}{c} \\ \\ \\ \end{array} \right)^2 = 0$$

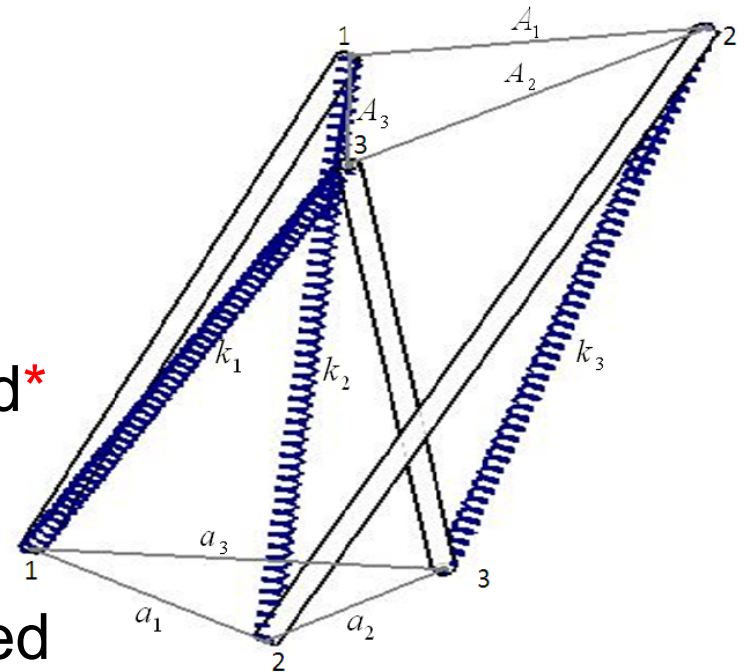
$$(X_{315}, Y_{315}, Z_{315})^{222} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} \quad \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}^2 = 0$$



Numerical Example

Three strut tensegrity

- $a_1=10$, $a_2=12.3$, $a_3 = 15$ cm
- $s_1 = 20$, $s_2 = 23$, $s_3 = 10.5$ cm
- $k_1 = 3.8$, $k_2 = 3$, $k_3 = 4.3$ N/cm
- The homotopy continuation method* was used to solve the set of 9 equations in 9 unknowns.
- 10 real configurations were obtained which satisfy the 9 equations (160 complex solutions obtained)



* PHCpack , <http://www.math.uic.edu/~jan/download.html>

Jan Verschelde, Univ. of Illinois at Chicago

Stability Analysis

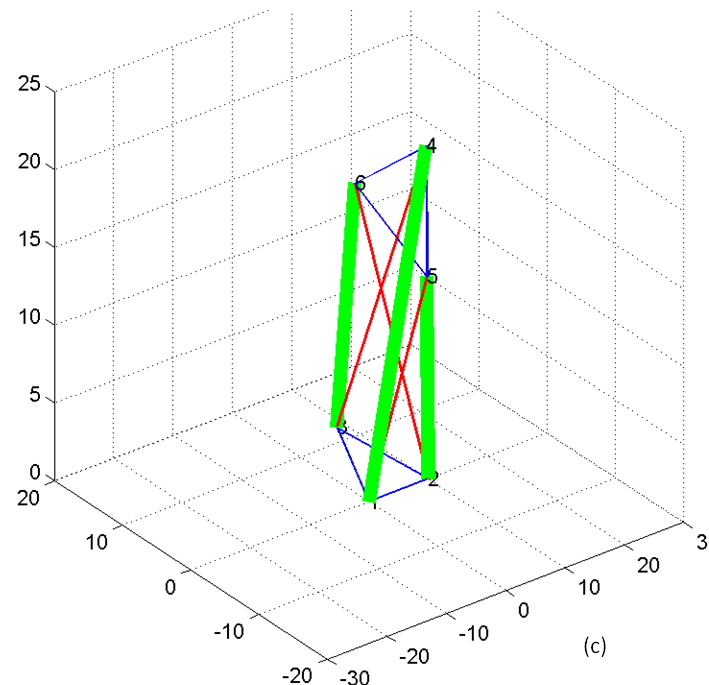
2nd Order Analysis

- A 2nd order analysis was conducted to classify the real solutions as
 - stable equilibrium
 - unstable equilibrium
 - neutral equilibrium
 - a small perturbation will continuously deform the structure to another neutral equilibrium state
 - have a statically balanced mechanism
- The equilibrium study becomes the examination of the positive definiteness of the Hessian matrix of the Lagrangian function w .

Numerical Example (cont)

stability analysis

- of the 10 real solutions
 - 1 is unstable (negative definite Hessian)
 - 7 are directionally stable (indefinite Hessian)
 - 2 are stable (positive definite Hessian)



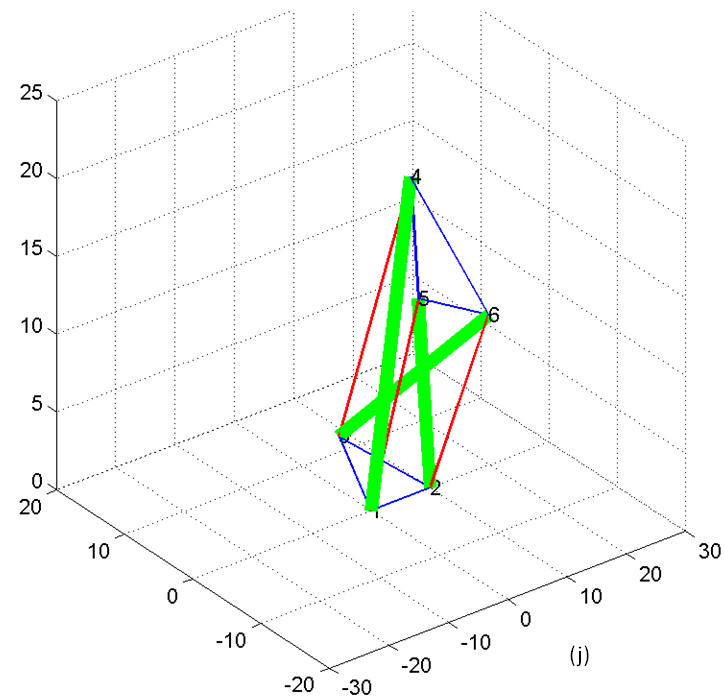
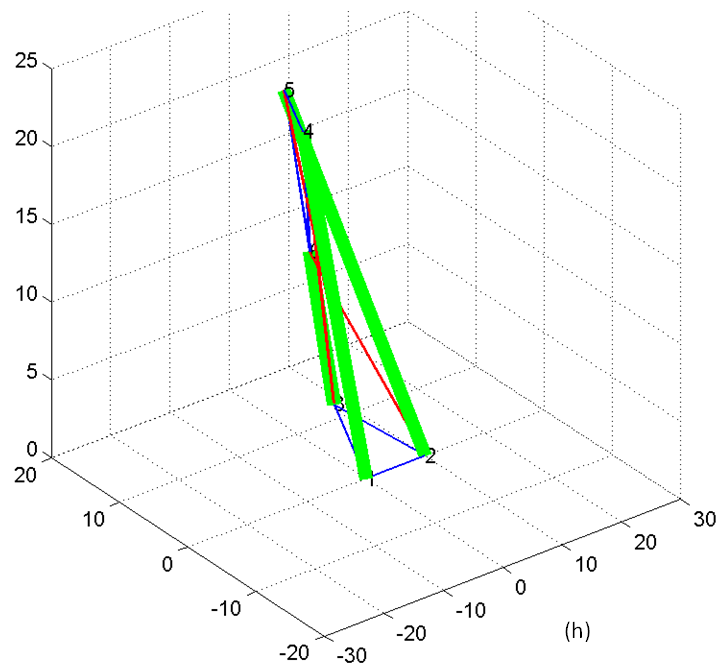
unstable case

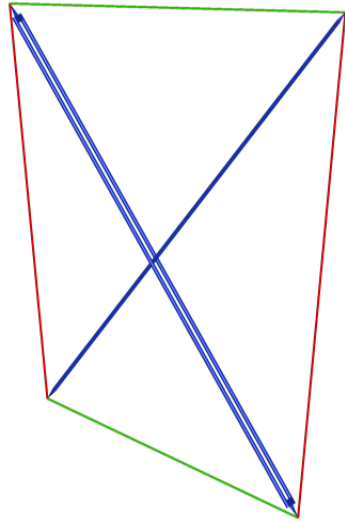
Numerical Example (cont)

stability analysis

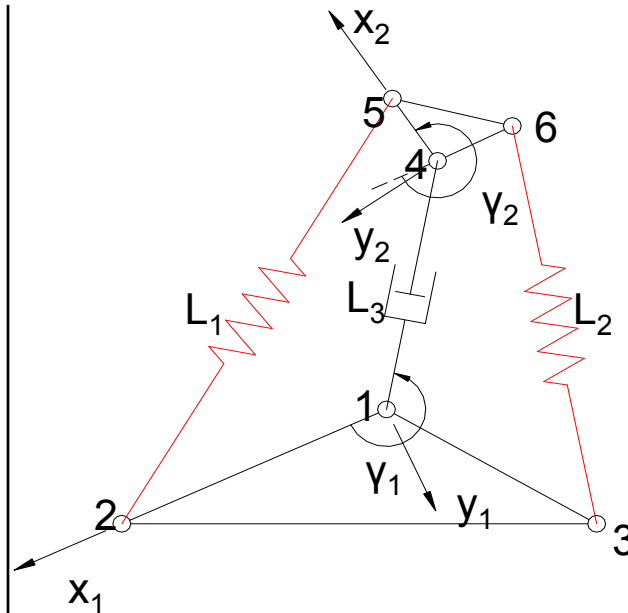
- of the 10 real solutions
 - 1 is unstable (negative definite Hessian)
 - 7 are directionally stable (indefinite Hessian)
 - 2 are stable (positive definite Hessian)

stable cases

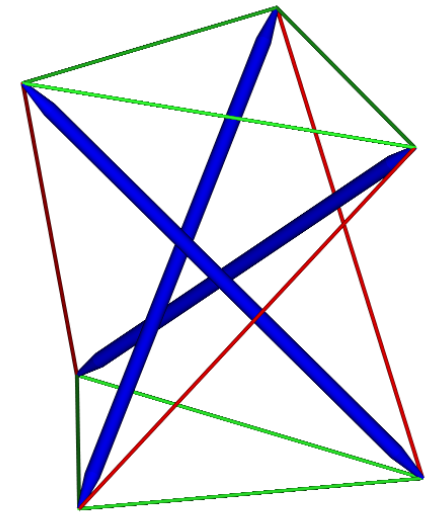




- 28th degree univariate polynomial
- numerical example had 8 real roots, 4 of which were stable equilibrium
- 1 of the 4 stable equilibrium had both spring lengths > 0



- Case 1, $L_{01} = L_{02} = 0$
 - 6 solutions, 4 real
- Case 2: $L_{02} = 0, L_{01} \neq 0$
 - 20 solutions, 8 real
- Case 3: $L_{02} \neq 0, L_{01} \neq 0$
 - 62 solutions, 24 real
 - problem formulation has extraneous roots



- free lengths equal zero
- 9 equations in 9 unknowns
- continuation method yielded 10 real and 160 complex solutions
- 2 cases were in stable equilibrium